# UPDATED TRANSPORTATION TECHNICAL REPORT 

# Fircrest School Master Development Plan 15230-15 ${ }^{\text {th }}$ Avenue NE, Shoreline, WA 

Washington State Department of Social \& Health Services


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## 1. INTRODUCTION

This report presents the transportation impact analyses for Washington State Department of Social and Health Services' (DSHS) proposed Fircrest School Master Development Plan (MDP) project, which will replace some of the existing buildings on campus and entitle an undeveloped south portion of the site for future development. This report documents the existing conditions in the site vicinity, presents estimates of project-related traffic, and evaluates the anticipated impacts to the surrounding transportation system including transit, parking, safety, and pedestrian facilities. The overall scope of this analysis was developed to provide details required by the City of Shoreline for a Traffic Impact Statement as outlined in the City of Shoreline's Traffic Study Guidelines ${ }^{1}$ and organized according to the City's Transportation Impact Analysis Report Guidelines. ${ }^{2}$ The approach, scope, and study area for the analysis were coordinated with City of Shoreline traffic review staff. ${ }^{3}$ This updated version of the report reflects additional information and revisions requested by the City of Shoreline in a comment memorandum ${ }^{4}$ and clarified in a follow-on meeting ${ }^{5}$ and subsequent email communications. ${ }^{6}$

At the time of this analysis, the COVID-19 pandemic and the changes it had on commuter behavior continued to affect traffic volumes and travel patterns throughout the region. Therefore, these analyses were prepared using a combination of baseline traffic data collected in 2018 prior to the pandemic and new data collected in January 2022. The data were adjusted to reflect normalized non-COVID conditions using standards and practices recommended by the Institute of Transportation Engineers (ITE), ${ }^{7}$ and other industry professionals. ${ }^{8}$

### 1.1. Project Description

### 1.1.1. Existing Campus

The Fircrest School site is located at $15230-15^{\text {th }}$ Avenue NE in the City of Shoreline. The overall site is bounded on the west by $15^{\text {th }}$ Avenue NE, on the north and northeast by Hamlin Park, on the east and southeast by Shorecrest High School and South Woods Park, and on the south by NE $150^{\text {th }}$ Street. It is designated as an Institution/Campus in the City's Comprehensive Plan on land zoned C (Campus). ${ }^{9}$ A rectangular area in the southeast portion of the site is noted as a Shoreline Park (the Eastside Off-Leash Area). The MDP does not propose changes to land use zoning or comprehensive designations; however, it would establish all of the permitted uses for the campus zoning based on the uses proposed in the MDP. About 12.5 acres located in the middle of the southern portion of the campus contain the Washington State Department of Health public health laboratory, which is not part of this MDP effort. Figure 1 shows the MDP area, which includes northern and eastern parts of campus; it does not consider the southwest corner of the DSHS property.

The Fircrest School MDP area currently has a total of 40 buildings (with about 429,000 square feet (sf)) on about 64.5 acres. The facility, which provides support to about 200 people with intellectual and developmental disabilities, was established in 1959 within a former Naval Hospital that later became a Tuberculosis Sanitarium. ${ }^{10}$

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Figure 1

## Fircrest School Master Development Plan

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The overall site program has three main components of care for persons with unique needs-1) Program Area Team skilled nursing facility (also known as PAT N); 2) the Adult Training Program (ATP), and 3) the residential element or Intermediate Care Facility for Individuals with Intellectual Disabilities (ICF/ID), also known as PAT A.

The PAT N facility is housed in six separate buildings, referred to as the ' Y ' buildings located at the northwest portion of the site. It provides individualized health care and activities to persons with unique medical needs and has 120 skilled nursing beds. The ATP is housed in six interconnected buildings located at the northeast portion of the site. It provides individualized habilitative services to support and enhance individual skills and strengths. The PAT A residential portion of the campus consists of 10 buildings. The buildings, referred to as 'the cottages,' are located in the central/eastern portion of the site and have 24-hour supervision with medical/nursing services. The ten PAT A cottages each have 16 beds; however, they currently house 133 patients with intellectual disabilities, which is considered full capacity.

In addition to the three main program elements, the site has support buildings that consist of a commissary, steam plant, kitchen, chapel, administrative / medical offices, office, activities building, maintenance, storage, warehouse, workshop, and gatehouse buildings. An on-site laundry building was destroyed by fire in July 2017 and has not yet been replaced. Traffic and parking generation at the campus is a function of the three primary program elements and the support buildings do not independently add traffic or parking needs. Table 1 lists the existing campus buildings, functions, and total sizes. The core trip-generating components are highlighted with one vacancy noted; the separate off-leash dog area is also noted as an existing trip-generating element.

Table 1. Fircrest School - Existing Building / Use Summary

| Type of Building / Function | Building \# | Area (sf) |
| :--- | :--- | ---: |
| 120-bed Nursing Facility ("Y" Buildings) | $55,56,57,58,59,60$ | $65,628 \mathrm{sf}$ |
| 16-bed ICF/ID Cottage (capacity of 133 patient / residents) | $44,45,46,47,48,49,50,51,52,53$ | $65,790 \mathrm{sf}$ |
| Administration/Medical Offices | 65 | $48,912 \mathrm{sf}$ |
| Building 66 (Vacant) | 66 | $41,046 \mathrm{sf}$ |
| Adult Training Program | $8586,87,88,89,90$ | $47,021 \mathrm{sf}$ |
| Kitchen | 39 | $21,950 \mathrm{sf}$ |
| Commissary | 24 | $8,000 \mathrm{sf}$ |
| Steam Plant | 28 | $8,256 \mathrm{sf}$ |
| Laundry | $31,32,33$ | $13,354 \mathrm{sf}$ |
| Chapel | 64 | $3,518 \mathrm{sf}$ |
| Activities Building | 67 | $35,341 \mathrm{sf}$ |
| Maintenance and Storage Buildings | $25,27,34,35,43,91$ | $34,794 \mathrm{sf}$ |
| Warehouse/Sheltered Workshop | 20,22 | $35,200 \mathrm{sf}$ |
| Gatehouse Building | 68 | 174 sf |
| Off-leash dog area |  | 1.4 acre |
| Total Building Area |  | $428,984 \mathrm{sf}$ |

Source: AHBL, November 2023
Current trip-generating site elements $\square$ Vacant trip-generating site element

Primary vehicular access to the campus is provided from $15^{\text {th }}$ Avenue NE at its signalized intersection with NE $155^{\text {th }}$ Street. The site can also be accessed from two driveways on NE $150^{\text {th }}$ Street-the eastern driveway opposite $20^{\text {th }}$ Avenue NE provides access to the undeveloped off-leash dog park and connects to the support-function buildings at the Fircrest School campus, and the western driveway is located
opposite $17^{\text {th }}$ Avenue NE and provides access to the Department of Health parcel. The western driveway from NE $150^{\text {th }}$ Street also connects internally to the Fircrest School campus near the southernmost PAT A residential cottage building. Automobile parking is provided near or adjacent to most buildings throughout the campus.

### 1.1.2. Master Development Plan Changes

The Fircrest School MDP is being prepared by DSHS to allow for the continued maintenance and redevelopment projects on the campus. The MDP envisions a range of permitted uses including:

| State-owned/operated office or laboratory; | Light industrial; |
| :--- | :--- |
| Medical-related office or clinic; | Food storage, warehousing and distribution; |
| Nursing facility; | Professional office; |
| Church, synagogue, temple; | Parks and trails; |
| Housing for disabled persons; | General retail trade, services; |
| Child and adult care services; | School district support facility (excluding vehicle |
| Library; | maintenance and storage); |
| Personal services; | Veterinary clinic \& hospital; |
| Social services provider; | Fire Station; and |
| Recreational facility; | Post Office. |
| Research development \& testing; |  |

For the purposes of this transportation impact analysis, the following elements have been assumed for the DSHS uses.

- Demolish the six existing " Y " buildings and construct a new 120 -bed skilled nursing facility.
- Site and construct a new 48 -bed ( $47,310 \mathrm{sf}$ ) behavioral health hospital facility.
- Demolish four of ten existing ICF/ID buildings and construct 14 new 4 bed ICF/ID cottages to provide for a total of 152 ICF/ID beds ( 96 existing and 56 new). Although full capacity will be maintained at 133 residents/patients, the traffic analysis evaluates conditions with 152 beds.
- Demolish the existing six ATP buildings and relocate the ATP into other existing buildings.
- Construct a new laundry building.
- Construct a new maintenance building.
- Construct a new commissary building
- Complete new internal circulation roadways.
- Expand surface parking within the site.
- Construct an addition ( $7,355 \mathrm{sf}$ ) to the existing activities building.

For the southeastern portion of the site a future commercial development is envisioned to be made-up of compatible uses and be developed by others. For this transportation analysis, it is assumed to consist of the following uses to reflect the highest (worst-case) level of trip generation.

- Medical/dental office building ( $85,000 \mathrm{sf}$ ) and a smaller general office building (28,320 sf) with a 5,000-sf daycare facility.
- The existing off-leash dog area would be removed, but publicly accessible open space is assumed within the southeast corner of the campus.
If any of the other envisioned uses are developed in the southern portion of the site instead, it is anticipated they would generate lower levels of traffic than evaluated herein. Table 2 lists the campus


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buildings, functions, and total sizes considered for the proposed MDP with the core trip-generating components highlighted. The existing buildings and functions are listed for comparison. The changes are expected to be completed in phases as funding is available, but may occur over 20 years. Figure 2 shows the proposed developments site plan.

As noted in Table 1 and Table 2, Building 66 is currently vacant. This is reflected in existing traffic counts that were performed at the site driveways. Standard practice for performing SEPA analyses is to assume that this building could be re-occupied in the future without the proposed project since no building permits would be required for such re-occupancy. The additional trips associated with re-use of Building 66 are included in both the 2042-without- and with-project traffic volumes.

Table 2. Fircrest School MDP - Building / Function Summary

| Existing Fircrest School Campus |  |  | Proposed Fircrest School MDP |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Building / Function | Building \# | Area (sf) | Building / Function | Building \# | Area (sf) |
| 120-bed Nursing Facility | $55,56,57,58,59,60$ | 65,628 sf | 120-bed Nursing Facility | New | 115,851 sf |
| 16-bed ICF/ID Cottages | $\begin{aligned} & 44,45,46,47,48 \\ & 49,50,51,52,53 \end{aligned}$ | 65,790 sf | 16-bed ICF/ID Cottages | 46, 47, 48, 49, 50, 51 | 39,474 sf |
| Administration / Medical Offices | 65 | 48,912 sf | 48-bed Behavioral Health Facility | New | 52,000 sf |
| Building 66 (Vacant) | 66 | 41,046 sf | 4-Bedroom ICF/ID Cottages - 14 buildings | New | 49,000 sf |
| Adult Training Program | $8586,87,88,89,90$ | 47,021 sf | Administration / Medical Offices | 65 | 48,912 sf |
| Kitchen | 39 | 21,950 sf | Administration Office ${ }^{1}$ | 66 | 41,046 sf |
| Commissary | 24 | 8,000 sf | Kitchen | 39 | 21,950 sf |
| Steam Plant | 28 | 8,256 sf | Commissary | New | 8,075 sf |
| Laundry | 31, 32, 33 | 13,354 sf | Chapel | 64 | 3,518 sf |
| Chapel | 64 | 3,518 sf | Activities Building | 67 | 35,341 sf |
| Activities Building | 67 | 35,341 sf | Activities Building Addition | New | 7,353 sf |
| Maintenance and Storage Buildings | 25, 27, 34, 35, 43, 91 | 34,794 sf | Warehouse / Sheltered Workshop | 20, 22 | 35,200 sf |
| Warehouse / Sheltered Workshop | 20, 22 | 35,200 sf | Gatehouse Building | 68 | 174 sf |
| Gatehouse Building | 68 | 174 sf | Laundry Facility | New | 15,000 sf |
| Off-leash dog area |  | 1.4 acre | Maintenance Facility | New | 42,794 sf |
|  |  |  | North Building Professional Office | New | 85,000 sf |
|  |  |  | South Building Professional Office ${ }^{2}$ | New | 28,320 sf |
| Total Building Area |  | 428,984 sf |  |  | 625,933 sf |

Source: AHBL, November 2023
Current trip-generating site elements $\square$ Vacant trip-generating site element $\square$

1. Although DSHS does not currently have plans to re-use this building, this analysis assumes it could be re-occupied as office space.
2. Analysis assumes 5,000 -sf daycare facility would be located in this building.


### 1.2. Project Location and Study Area

As stated previously, the site is located at $15230-15^{\text {th }}$ Avenue NE in the City of Shoreline. Vehicular access to the site would occur from two locations-the primary main campus access would remain from the existing signalized access driveway on $15^{\text {th }}$ Avenue NE opposite NE $155^{\text {th }}$ Street. The new development at the southeast corner would be accessed from a new driveway on NE $150^{\text {th }}$ Street located about 290 feet west of $20^{\text {th }}$ Avenue NE. The eastern most driveway on NE $150^{\text {th }}$ Street would be removed; the western access located opposite $17^{\text {th }}$ Avenue NE and providing access to the Department of Health parcel would remain but would no longer connect internally to the Fircrest Campus. An existing gated access on $15^{\text {th }}$ Avenue NE about 350 feet north of NE $155^{\text {th }}$ Street is planned to be retained, but remain gated with access limited to emergency and/or maintenance vehicles.

The City of Shoreline's Traffic Study Guidelines indicate that a development of the size and scale proposed (estimated to generate between 100 and 500 peak hour trips), is required to evaluate site access points and nearby intersections. Based on scope coordination with the City of Shoreline Traffic Engineer, ${ }^{11}$ the following off-site study-area intersections were selected for review in addition to site access. Figure 3 shows the project site location and vicinity street system.

## Signalized Intersection

1. NE $155^{\text {th }}$ Street $/ 5^{\text {th }}$ Avenue NE
2. NE $155^{\text {th }}$ Street $/ 15^{\text {th }}$ Avenue NE
3. NE $150^{\text {th }}$ Street $/ 15^{\text {th }}$ Avenue NE

## Unsignalized Intersections

4. NE $150^{\text {th }}$ Street $/ 25^{\text {th }}$ Avenue NE
5. NE $150^{\text {th }}$ St $/$ Fircrest School Access $/ 20^{\text {th }}$ Ave NE

[^1]

### 1.3. Summary of Findings

The following summarizes the findings of the transportation analysis:

- The changes in program envisioned by MDP are estimated to generate net increases of up to 3,710 daily trips; 383 AM peak hour trips, and 498 PM peak hour trips.
- New traffic generated by MDP development would add delay to study-area intersections during the AM and PM peak hours. All of the signalized study-area intersections are projected to operate at LOS E or better with the proposed project. However, the all-way-stop-controlled NE $150^{\text {th }}$ Street / $25^{\text {th }}$ Avenue NE intersection is forecast to degrade to LOS F by 2042 without the project, and would be exacerbated by additional project traffic if no changes to traffic control are made.
- The site access driveway on NE $150^{\text {th }}$ Street is forecast to operate at LOS A overall with all movements operating at LOS C or better.
- The MDP proposes 812 parking spaces allocated throughout the campus (an increase of 271 spaces compared to existing conditions). The planned supply is expected to exceed the estimated parking demand for the campus which is estimated at 746 vehicles. Parking supply for the individual masterplan elements would be determined at the time of permit application, and the number of spaces needed will depend on the intended building program.


### 1.4. Summary of Recommended Mitigation

The following measures have been incorporated into the project proposal and/or are recommended to minimize the traffic and parking impacts associated with the Fircrest School MDP.
A. Construction Transportation Management Plan (CTMP) - DSHS should require the selected contractor to develop a CTMP. The elements of the CTMP are described in detail in Section 4.
B. Travel Demand Management Plan (TDMP) - A TDMP is a standard requirement for MDPs in the City of Shoreline. The TDMP for the Fircrest Campus would evolve as the individual elements are implemented and as owner/operators are identified.
C. Contribute to cost of improvements (e.g., signalization or conversion to roundabout) at NE $\mathbf{1 5 0}{ }^{\text {th }}$ Street $/ \mathbf{2 5}^{\text {th }}$ Avenue NE - It would also be appropriate for the project to contribute a proportionate share (estimated at between $2.7 \%$ and $3.4 \%$ ) toward the costs of operational improvements (such as signalization or conversion to roundabout) to mitigate its impacts, if the improvement is not incorporated into the City's Transportation Impact Fee system.
D. Signal optimization for NE $\mathbf{1 5 5}^{\mathbf{t h}}$ Street $/ \mathbf{1 5}^{\text {th }}$ Avenue NE intersection - It may be desirable to implement operational changes at this intersection. If requested by the City, the project could contribute a proportionate share (estimated at up to $11 \%$ ) toward the costs of the signal optimization and channelization re-striping improvements, if these improvements are not incorporated into the City's Transportation Impact Fee system.
E. Parking analysis at time of development permitting - Parking supply for each individual MDP element would be determined at the time of permit application, and the number of spaces needed will depend on the intended building program. It is expected that sufficient supply would be provided to meet project parking demand. If future demand is estimated to exceed the supply, then the proponent should be required to perform further studies to determine if parking mitigation (e.g., share parking or trip reduction strategies) would be needed.

In addition to the recommended measures above, the City of Shoreline collects Transportation Impact Fees (TIFs) from applicants seeking building permits for either new developments or changes of use. Based on the above, the potential TIF for all contemplated MDP uses could range from about \$3,342,000 ( $\$ 490,600$ for DSHS Program elements and $\$ 2,851,400$ for other commercial elements) to $\$ 4,144,500$ ( $\$ 857,200$ for DSHS Program elements and $\$ 3,287,300$ for other commercial elements). It is noted that TIFs are collected at the time of building permit issuance and at the rates in place at that time.

## 2. BACKGROUND CONDITIONS

This section of the report presents the existing and future conditions without the proposed Fircrest School MDP. The impacts of the proposed project were evaluated against these base conditions. DSHS expects that the MDP project elements may be completed over the next 20 years; therefore, year 2042 was selected as the future horizon year for this analysis. The following sections describe the existing roadway network, traffic volumes, traffic operations (in terms of levels of service), traffic safety, transit facilities, and pedestrian/bicycle (non-motorized) facilities.

### 2.1. Roadway Network

The project site is located on the east side of $15^{\text {th }}$ Avenue NE between about NE $160^{\text {th }}$ and NE $150^{\text {th }}$ Streets. The primary roadways that serve the site and its vicinity are $15^{\text {th }}$ Avenue NE, NE $155^{\text {th }}$ Street, and NE $150^{\text {th }}$ Street. The following provides a description of the study area roadways ${ }^{12}$.
$15^{\text {th }}$ Avenue NE is a north-south Principal Arterial connecting the south City limit at NE $145^{\text {th }}$ Street to the north City limit at NE $205^{\text {th }}$ Street. Within the study area, the roadway has two travel lanes (one in each direction) plus a center, two-way, left-turn lane and bicycle lanes on both sides. It has curbs on both sides and sidewalk along the west side. The posted speed limit is 35 miles per hour (mph). Its intersections at NE $150^{\text {th }}$, NE $155^{\text {th }}$, NE $160^{\text {th }}$, and NE $165^{\text {th }}$ Street are signalized.

NE $\mathbf{1 5 0}^{\text {th }}$ Street is an east-west roadway designated as a Collector Arterial near the site (from $15^{\text {th }}$ to $25^{\text {th }}$ Avenue NE). East of $25^{\text {th }}$ Avenue NE, it is a Local Secondary Street terminating at $28^{\text {th }}$ Avenue NE. Adjacent to the site, it has one lane in each direction with curb and walkway (concrete and asphalt) on the north side and bicycle lanes on both sides. The posted speed limit is 30 mph . Its intersection with $15^{\text {th }}$ Avenue NE is signalized; its intersection with $25^{\text {th }}$ Avenue NE is all-way-stop controlled.

NE $155^{\text {th }}$ Street is an east-west roadway designated as a Minor Arterial and connecting Aurora Avenue N on the west and $15^{\text {th }}$ Avenue NE on the east. Near the site, the roadway has two travel lanes (one in each direction) plus a center, two-way, left-turn lane and bicycle lanes on both sides. It has curbs and sidewalks on both sides. East of $15^{\text {th }}$ Avenue NE, the street becomes the main internal access road for the Fircrest School site. The posted speed limit is 30 mph . Its intersection with $15^{\text {th }}$ Avenue NE and the Fircrest School access is signalized.

NE $165^{\text {th }}$ Street is an east-west Collector Arterial between $5^{\text {th }}$ and $15^{\text {th }}$ Avenues NE. It has one travel lane in each direction, with curb and sidewalk on the north side. The posted speed limit is 25 mph . On-street parallel parking occurs along some segments on both sides. Its intersection with $15^{\text {th }}$ Avenue NE is signalized. East of $15^{\text {th }}$ Avenue NE, it is a dead-end local street.
$25^{\text {th }}$ Avenue NE is a north-south Collector Arterial that extends north from the south City limit to NE $168^{\text {th }}$ Street and then continues in segments to NE $178^{\text {th }}$ Street. In the site vicinity, it has one travel lane in each direction, parking east side of the street, with curb and sidewalk on both sides. The posted speed limit is 30 mph ; however, there are 20 mph school zones in several locations (near Shoreline Christian School, Shorecrest High School, and Kellogg Middle School). Its intersection with NE $150^{\text {th }}$ Street is all-way-stop controlled.

At the time of this report, the City of Shoreline was actively engaged in a multi-year process to update its Transportation Master Plan (TMP). The City of Shoreline's most recent available TMP, 2011 Transportation Master Plan (TMP), was reviewed. Several planned improvements would provide designated bicycle lanes on $15^{\text {th }}$ Avenue NE, NE $155^{\text {th }}$ Street, and extensions of existing bicycle lanes on $15^{\text {th }}$ Avenue NE. The plan also calls for the designation of a signed bicycle route along NE $160^{\text {th }}$ Street

12 City of Shoreline, Street Classification, October 2019.

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north of the project site. Finally, the plan identifies the segments of NE $150^{\text {th }}$ Street and $15^{\text {th }}$ Avenue NE adjacent to the project site as part of the proposed pedestrian system with sidewalk improvements identified to fill in missing segments or gaps.

The City of Shoreline's 2024 to 2029 Transportation Improvement Program (TIP), ${ }^{13}$ its 2023-2024 Capital Improvement Plan (CIP) ${ }^{14}$ and its 2023 Capital Improvement Project Map ${ }^{15}$ were also reviewed to determine if there are funded transportation improvements scheduled in the study area. The TIP and 2023 CIP Map identify sidewalk improvements along $15^{\text {th }}$ Avenue NE adjacent to the project site.

Based on review of the CIP, TIP, and other planning documents, no other specific changes are expected to affect the operational capacity of the study area roadways and intersections for the forecast year 2042 analysis conditions. Therefore, the existing roadway channelization and traffic control were assumed for all future conditions analyses.

### 2.2. Traffic Volumes

New AM and PM peak period video turning movement counts were conducted by Idax Data Solutions at all study-area intersections on January 11, 2022. In addition, the counts performed previously at four study intersections for this project on September 27, 2018 and at the two remaining study intersections for another project on May 31, 2018 (all by Idax) were compiled for review.

Based on comparisons of data from 2018 and 2022, current traffic volumes at most locations have not rebounded from the declines caused by the COVID-19 pandemic. At comparable locations, total entering PM peak hour volumes in 2022 ranged from about $47 \%$ to about $79 \%$ of the 2018 volumes; total entering AM peak hour volumes in 2022 ranged from $56 \%$ to $91 \%$ of the 2018 levels. These levels are consistent with count data throughout the region and account for the large number of employees that continue to work from home. An exception was the volumes along NE $150^{\text {th }}$ Street between $15^{\text {th }}$ and $25^{\text {th }}$ Avenues NE where AM peak hour volumes in 2022 were higher than in 2018. The increase is likely due to the fact that the State Health Lab increased staff to perform COVID testing. Based on the above data review and with guidance from City of Shoreline Traffic Engineering staff, normalized 2022 non-COVID peak hour volumes were derived using the higher of 2018 and 2022 movement volumes at each study intersection. Figure 4 shows the estimated existing (2022) normalized peak hour traffic volumes at the study area intersections for the AM and PM peak hours, respectively.

The Fircrest School MDP elements may be completed over 20 years; therefore, the analysis was performed for year 2042 conditions. Consistent with other analyses prepared for projects in the City of Shoreline, compound annual growth rates for the arterials in the study area were derived from growth projections in the City's 2011 Transportation Master Plan. The growth projections reflect potential increases in PM peak hour traffic between the base model year (2008) and 2030. A comparison of the growth projections indicate study-area intersections could experience compound annual increases ranging up to $3.1 \%$ with most locations expected to grow by $0.3 \%$ to $2 \%$ annually. The derived growth rates were applied to the existing traffic volumes to estimate 2042 volumes without the project. Pipeline development traffic from one project-AAA $149^{\text {th }}$ Apartments-was provided by the City ${ }^{16}$ and added to the forecasts. Finally, traffic that could be generated by the Fircrest School site, if existing vacant buildings were re-occupied (described later in Section 3.2), was also added to background traffic conditions. Figure 5 shows the forecast 2042-without-project traffic volumes for the AM and PM peak hours, respectively.

[^2]

Fircrest School Master Plan Traffic Impact Statement

Figure 4
Existing (2022) Normalized Traffic Volumes
AM and PM Peak Hours


Figure 5
Forecast (2042) Without-Project Traffic Volumes AM and PM Peak Hours

Fircrest School Master Plan Traffic Impact Statement

### 2.3. Traffic Operations

Traffic operations analysis was performed for the study area intersections described previously. Traffic operations are evaluated using level of service (LOS) with six letter designations, "A" through "F." LOS A is the best and represents good traffic operations with little or no delay to motorists. LOS F is the worst and indicates poor traffic operations with long delays.

The City of Shoreline has adopted LOS D as its standard for signalized intersections on arterials and unsignalized intersecting arterials for review of traffic impacts of developments. ${ }^{17}$ In addition, a supplemental LOS standard "for Principal Arterials and Minor Arterials limits the volume to capacity ( $\mathrm{v} / \mathrm{c}$ ) ratio to 0.90 or lower, provided the $\mathrm{v} / \mathrm{c}$ ratio on any leg of a Principal or Minor Arterial intersection may be greater than 0.90 if the intersection operates at LOS D or better." These LOS standards apply throughout the city except where an alternate standard has been adopted for Principal or Minor Arterial segments where "widening the roadway cross-section is not feasible, due to significant topographic constraints; or rechannelization and safety improvements result in acceptable levels of increased congestion in light of the improved operational safety of the roadway." One of the arterial segments meeting at least one of these criteria is $15^{\text {th }}$ Avenue NE from N $150^{\text {th }}$ Street to N $175^{\text {th }}$ Street where the v $/ \mathrm{c}$ may not exceed 1.10.

It is noted that the City of Shoreline is currently in the process of preparing a Transportation Master Plan Update to the current 2011 version. The City is in Outreach Series 3 and is soliciting community feedback on draft plans for various travel modes (auto, transit, pedestrian, and bicycle). The draft plan suggests a possible small increase in travel delay policy for automobiles along $15^{\text {th }}$ Avenue NE from NE $155^{\text {th }}$ to the south City limits. As a result, LOS standards may be revised prior to development of the MDP elements. The level of service definitions and thresholds are in the Appendix A.

Levels of service for the study area intersections were determined using procedures in the Highway Capacity Manual $6^{\text {th }}$ Edition. ${ }^{18}$ All level of service calculations were performed using the Synchro 10.1 traffic operations analysis software, using the Synchro reporting module for the signalized intersection and the HCM 6 reporting module for unsignalized intersections. The PM peak hour analyses reflect existing signal timings provided by the City of Shoreline; the AM peak hour analyses reflect modified signal phase splits to account for morning volume patterns. Table 3 summarizes existing and 2042-without-project levels of service. The LOS calculation sheets are provided in Appendix B.

As shown, the three signalized intersections currently operate at LOS D or better overall during AM and PM peak hours. The all-way-stop-controlled NE $150^{\text {th }}$ Street $/ 25^{\text {th }}$ Avenue NE intersection operates at LOS E in the morning and LOS C in the afternoon. The NE $150^{\text {th }}$ Street / $20^{\text {th }}$ Avenue NE intersection operates at LOS A overall with all movements at LOS C or better during both peak hours.

The assumed growth in background traffic is expected to add delay and cause some degradation to operations at the three signalized intersections, but all three are forecast to remain operating at LOS D or better. The growth assumed for the all-way-stop-controlled NE $150^{\text {th }}$ Street $/ 25^{\text {th }}$ Avenue NE intersection is forecast to degrade operations to LOS F during both AM and PM peak hours by 2042. Based on these levels of delay, a change to traffic control (signalization or conversion to a roundabout) may be required and could improve operations to LOS C or better. The forecast volumes and levels of delay would meet the peak hour warrant (Warrant 3) for signalization outlined in the Manual on Uniform Traffic Control Devices (MUTCD) for Streets and Highways. ${ }^{19}$ However, City review and monitoring would be needed to determine the intersection meets warrants for signalization or alternative traffic control measures, such as conversion to roundabout.

[^3]Table 3. Intersection Level of Service Summary - Existing and Forecast 2042 Background

| Intersection Type / Location | AM Peak Hour |  |  |  |  |  | PM Peak Hour |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Existing |  |  | Without Project |  |  | Existing |  |  | Without Project |  |  |
| Signalized Intersections | LOS ${ }^{1}$ | Delay ${ }^{2}$ | v/c ${ }^{3}$ | LOS | Delay | v/c | LOS | Delay | v/c | LOS | Delay | v/c |
| 1. NE 155th St / $5^{\text {th }}$ Ave NE | B | 18.4 | 0.81 | C | 22.1 | 0.85 | B | 18.3 | 0.77 | C | 33.2 | 0.99 |
| 2. NE 155 ${ }^{\text {th }}$ St / 15 ${ }^{\text {th }}$ Ave NE | B | 16.2 | 0.75 | C | 32.9 | 1.00 | C | 23.8 | 0.89 | D | 36.9 | 1.01 |
| 3. NE 150 ${ }^{\text {th }}$ St $/ 15^{\text {th }}$ Ave NE | B | 16.9 | 0.77 | B | 17.2 | 0.78 | B | 16.4 | 0.70 | B | 18.9 | 0.70 |
| All-Way-Stop Intersection | LOS | Delay | v/c | LOS | Delay | v/c | LOS | Delay | v/c | LOS | Delay | v/c |
| 4. NE 150 ${ }^{\text {th }}$ St $/ 25^{\text {th }}$ Ave NE | E | 47.5 |  | F | 126.5 |  | C | 17.7 |  | F | 83.2 |  |
| Northbound Movements | C | 17.7 | 0.52 | E | 39.8 | 0.92 | B | 13.1 | 0.76 | F | 137.7 | 1.22 |
| Eastbound Left Turns | D | 25.6 | 0.73 | F | 143.9 | 1.32 | A | 9.9 | 0.41 | C | 24.7 | 0.75 |
| Westbound Left Turns | B | 14.6 | 0.31 | C | 19.5 | 0.42 | C | 23.0 | 0.06 | B | 11.8 | 0.07 |
| Southbound Movements | F | 80.8 | 1.05 | F | 182.8 | 1.41 | B | 11.1 | 0.34 | B | 14.3 | 0.44 |
| Stop Controlled Intersection | LOS | Delay | v/c | LOS | Delay | v/c | LOS | Delay | v/c | LOS | Delay | v/c |
| 5. NE 150 ${ }^{\text {th }}$ St $/ 20^{\text {th }}$ Ave NE | A | 2.0 |  | A | 2.6 |  | A | 3.8 |  | A | 4.3 |  |
| Northbound Movements | B | 14.7 | 0.14 | C | 19.0 | 0.23 | B | 12.0 | 0.22 | B | 14.1 | 0.31 |
| Eastbound Left Turns | A | 7.9 | 0.01 | A | 8.1 | 0.01 | A | 7.5 | 0.00 | A | 7.6 | 0.00 |
| Westbound Left Turns | A | 8.2 | 0.02 | A | 8.4 | 0.03 | A | 7.8 | 0.01 | A | 8.0 | 0.01 |
| Southbound Movements | C | 16.7 | 0.09 | C | 22.0 | 0.15 | B | 11.5 | 0.06 | B | 12.8 | 0.09 |

Source: Heffron Transportation, Inc., April 2022.

1. LOS = Level of service. LOS E shaded $\square$ LOS F shaded $\square$;
2. $\quad$ Delay $=$ Average delay per vehicle in seconds.
3. $\quad$ Maximum reported $v / c=$ Volume-to-capacity ratio for lane group.

### 2.4. Traffic Safety

Collision data for the study-area intersections and roadway segments adjacent to the site were obtained from the Washington State Department of Transportation (WSDOT). These data, reflecting the period between January 1, 2018 and the most recent available, December 20, 2021 (about four years), were examined to determine if there are any unusual traffic safety conditions that could impact or be impacted by the proposed project. The collision data are summarized in Table 4. As shown, all of the study-area intersections averaged fewer than three collisions per year.

The City of Shoreline's Annual Traffic Report, 2020 was also reviewed for this analysis. The report summarizes High Collision Locations (HCLs) based on various criteria. The 2020 report made special note in its executive summary that total crashes nationwide decreased during the COVID-19 pandemic, the rate of fatal crashes increased. The report identifies nine intersections and three roadway segments city-wide that had the highest number of collisions experienced during the three-year period between 2018 and 2020. Locations with three or more pedestrian collisions or two or more bicycle collisions over a five-year period between 2016 and 2020 are also listed in the report. None of the study-area intersections were listed in the City's Annual Traffic Report as HCLs; a portion of the segment along $15^{\text {th }}$ Avenue NE (from NE $150^{\text {th }}$ Street to NE $155^{\text {th }}$ Street) was identified in the report as a corridor location to continue to monitor.

Table 4. Historical Collision Summary - January 1, 2018 - December 20, 2021 (4 years)

| Intersections | Number of Collisions by Type |  |  |  |  |  | Total (4 Yrs) | Avg I |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | RearEnd | Side <br> Swipe | Left Turn | Right <br> Angle | Ped I Cycle | Other ${ }^{\text {a }}$ |  |  |
| Signalized |  |  |  |  |  |  |  |  |
| NE 150 ${ }^{\text {th }}$ St / $15^{\text {th }}$ Ave NE | 3 | 0 | 1 | 3 | 1 | 0 | 8 | 2.0 |
| NE 155 ${ }^{\text {th }}$ St / $15^{\text {th }}$ Ave NE | 3 | 0 | 3 | 2 | 0 | 0 | 8 | 2.0 |
| NE 155 ${ }^{\text {th }}$ St / 5 ${ }^{\text {th }}$ Ave NE | 0 | 0 | 2 | 3 | 0 | 1 | 6 | 1.5 |
| All-Way Stop-Controlled |  |  |  |  |  |  |  |  |
| NE 150 ${ }^{\text {th }}$ St $/ 25^{\text {th }}$ Ave NE | 1 | 0 | 0 | 3 | 0 | 1 | 5 | 1.3 |
| Two-Way Stop-Controlled |  |  |  |  |  |  |  |  |
| NE $150^{\text {th }}$ St / $20^{\text {th }}$ Ave NE / Fircrest School Access | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.0. |
| Roadway Segments | Rear- <br> End | Side <br> Swipe | Left <br> Turn | Right <br> Angle | Ped I <br> Cycle | Other ${ }^{\text {a }}$ | Total (4 Yrs) | Avgl <br> Year |
| NE 150th St, between $15^{\text {th }}$ Ave NE and $25^{\text {th }}$ Ave NE | 0 | 0 | 0 | 1 | 0 | 1 | 2 | 0.5 |
| $15^{\text {th }}$ Ave NE, between NE 158 ${ }^{\text {th }}$ St and NE 150th St | 4 | 1 | 0 | 1 | 0 | 4 | 10 | 2.5 |

Source: $\quad$ WSDOT, January 2022. Reflect collision data for the 4.0-year time period between January 1, 2018 and approximately December 20, 2021. Collisions that occurred recently during the study period (within the past 30 days) may not have been entered into the WSDOT database.
a. "Other" collisions were two vehicles struck fixed objects in the roadway, two vehicles struck fixed objects off the roadway, one vehicle struck a fixed object, and one vehicle struck a parked vehicle.

There was one recorded pedestrian collision at the NE $150^{\text {th }}$ Street $/ 15^{\text {th }}$ Avenue NE intersection. The collision occurred on Wednesday, December 15, 2021 and the contributing cause was cited as the driver's failure 'to yield right-of-way to pedestrian. There was one collision involving two vehicles that resulted in a fatality (on May 31, 2020) at the NE $155^{\text {th }}$ Street $/ 5^{\text {th }}$ Avenue NE. A contributing factor listed was "disregard for traffic signs and signals."

### 2.5. Transit

The site is served by King County Metro Transit Routes 330 and 348 . Route 348 operates along $15^{\text {th }}$ Avenue NE adjacent to the site; Route 330 operates along NE $150^{\text {th }}$ Street, $25^{\text {th }}$ Avenue NE, and NE $155^{\text {th }}$ Street. Route 330 provides weekday peak period directional service between Lake City and Shoreline Community College. Route 348 operates full-day service, 7 days per week, to and from Richmond Beach, Shoreline, Northgate, North City, Shoreline, Ballinger, and Mountlake Terrace. The headways (time between consecutive buses) range between 10 and 60 minutes. The closest stops are located adjacent to the site on $15^{\text {th }}$ Avenue NE at its intersection with NE $155^{\text {th }}$ Street.

Less than a mile to the west of the Fircrest School site, Sound Transit is constructing the $148^{\text {th }}$ Street Transit Station as part of the Lynnwood Link Light Rail Extension project. Located just northeast of I-5 at the NE $145^{\text {th }}$ Street exit, the elevated Shoreline Station will be served by Link light rail beginning in 2024 with frequent service between south Snohomish County and the University of Washington, downtown Seattle, the Eastside, Sea-Tac Airport, and beyond. It will also provide a connection to the new the Sound Transit SR 522/NE $145^{\text {th }}$ Bus Rapid Transit service, which is also scheduled to begin service in 2024.

### 2.6. Non-Motorized Transportation Facilities

As described in Roadway Network section (2.1), there are intermittent pedestrian and bicycle facilities within the study area. Near the project site, there is sidewalk along the west side of $15^{\text {th }}$ Avenue NE and bicycle lanes on both sides. However, there are only intermittent segments of sidewalk along the east side of $15^{\text {th }}$ Avenue NE, but there is a narrow, foot-worn path in the grass behind a vertical curb. There is curb and sidewalk along the north side of NE $150^{\text {th }}$ Street near the site and bicycle lanes on both sides. There are curbs, sidewalks, and bicycle lanes on both sides of NE $155^{\text {th }}$ Street.

Crosswalks and pedestrian crossing signals are provided on all legs of the signalized study intersections; there are marked crosswalks on all legs of the unsignalized NE $150^{\text {th }}$ Street $/ 25^{\text {th }}$ Avenue NE intersections

As described previously, the City of Shoreline plans to construct sidewalk along the east side of $15^{\text {th }}$ Avenue NE north of NE $150^{\text {th }}$ Street.

## 3. TRAFFIC IMPACTS

This section of the report describes the conditions that could exist with the proposed Fircrest School MDP elements complete and occupied. The following sections describe the methodology used to determine the proposed project's impacts and the results of the analysis. As described previously, year 2042 was selected as the future horizon year for this analysis to represent conditions when all elements of the MDP could be complete and occupied.

### 3.1. Roadway Network

With the changes contemplated by the MDP, vehicular access to the site would occur from two locations-the primary Fircrest School campus access would remain from the existing signalized access driveway on $15^{\text {th }}$ Avenue NE opposite NE $155^{\text {th }}$ Street. An existing gated access on $15^{\text {th }}$ Avenue NE about 350 feet north of NE $155^{\text {th }}$ Street is planned to be retained, but remain gated with access limited to emergency and/or maintenance vehicles. The new development at the southeast corner would be accessed from a new driveway on NE $150^{\text {th }}$ Street located about 290 feet west of $20^{\text {th }}$ Avenue NE. The eastern most driveway on NE $150^{\text {th }}$ Street would be removed. Frontage improvements would be constructed along the portions of campus included in the MDP and are proposed to be completed in phases with triggers based on campus improvements. No other changes to the existing off-site roadway network are proposed.

### 3.2. Traffic Volumes

The City requires that trip generation estimates be developed using rates and equations published by the Institute of Transportation Engineers (ITE) in its most current edition of the Trip Generation Manual. ${ }^{20}$ Trip estimates for each site component were prepared based on their current and/or expected function and the best-fit uses included in the ITE manual. Trip generation models for the overall site were prepared for existing and future conditions and then compared to estimate the net change in traffic generation that could occur with the MDP.

### 3.2.1. Selected Trip Generation Rates and Equations

Based on the existing and proposed facilities and functions that make up the Fircrest School Campus, the ITE land use categories that were selected to estimate trip generation are described for each component.

ICF/ID Cottages: Assisted Living (Land Use 254) - This land use is a "residential setting that provides either routine general protective oversight or assistance with activities necessary for independent living to persons with mental or physical limitations. The typical resident has difficulty managing in an independent living arrangement but does not require nursing home care. Its centralized services typically include dining, housekeeping, social and physical activities, medication administration, and communal transportation. The complex commonly provides separate living quarters for each resident." This best matches the existing and planned future ICF/ID cottages within the campus.

PAT N Nursing Facility: Nursing Home (Land Use 620) - This land use is described as "...a facility whose primary function is to provide care for persons who are unable to care for themselves. Examples include rest homes, chronic care, and convalescent homes. Skilled nurses and nursing aides are present 24 hours a day at these sites. Residents often require treatment from a registered healthcare professional for ongoing medical issues. A nursing home resident is not capable of operating a vehicle. Traffic is

[^4]entirely generated by employees, visitors, and deliveries." This best matches the existing and future PAT N nursing facility component.

Administration Offices: Single-Tenant Office Building (Land Use 715) - This land use is described as a building that "...generally contains offices, meeting rooms, and space for file storage and data processing of a single business or company and possibly other service functions including a restaurant or cafeteria." This category is best for application to the existing and future Fircrest School administration office buildings within the campus.

Behavior Health Hospital: Hospital (Land Use 610) - There is no ITE category that exactly reflects the planned behavioral health hospital. The facility proposed as part of the MDP would have 48 beds with up to 400 employees. The facility would be staffed seven days per week with three shifts operating 24-hours per day. There would be limited turn-over of patients and the facility would not be open to the public with ingress and egress mainly by staff and physicians. ITE's Hospital land use is the most similar to the proposed facility. After review of the three possible independent variables that could be applied, guidance published by ITE in its Trip Generation Manual on selecting independent variables, and expected staffing and shift information provided by the applicant, peak hour rates based on gross floor area were selected. These rates are based on the largest number of studies and have a data point near the size of the proposed project. The resulting peak hour trip estimates are consistent with traffic patterns that would be expected based on the staffing, shift details, and operational expectations provided by the applicant. In contrast, the published rates based on number of beds were derived from only seven studies, with none near the proposed number for this site. Trip estimates based on number of employees were also reviewed and determined to be unreasonable; the peak hour rates based on employees resulted in trips that appeared to be too high given the same staffing and operational parameters. This traffic analysis approach has been applied and accepted recently for a behavioral health hospital project in Lacey, Washington. ${ }^{21}$

North Professional Office Building: Medical-Dental Office Building (LU 720) - The anticipated worst-case use, in terms of trip generation, for the larger of the two new professional office buildings (planned to be developed by others) at the southeast part of the site would be as a medical/dental office building.

South Professional Office Building: General Office Building (LU 710) and Daycare Center (Land Use 565) - The smaller of the two new professional office buildings planned (to be developed by others) at the southeast part of the site was assumed to be a general office building that also contains at $5,000-\mathrm{sf}$ daycare center. The daycare center is expected to give priority to employees who work in the building, the adjacent north office building, and/or the larger Fircrest School site, similar to daycare facilities that the state built near the Capitol Campus in Olympia. Therefore, $50 \%$ of its trips were assumed to be the same as those generated by other uses on site-employees coming to the site who also bring their children to the daycare center. A $50 \%$ rate of external daycare use is likely conservative, since nearly all of the children enrolled in the planned facility would arrive in the same vehicles as the employees on the site. Even with the $50 \%$ adjustment, the number of new trips generated by this MDP element are likely overstated.

Off-Leash Dog Area: There are no published ITE rates to estimate trip generation by off-leash dog areas. Therefore, trip estimates for this existing use were derived using a rate derived by Heffron Transportation, and presented in the Transportation Impact Analysis for Off-Leash Dog Area(s) at the Chambers Creek Properties. ${ }^{22}$ The weekday PM peak hour rate was developed from counts and

[^5]observations at three off-leash areas (Grandview, Marymoor, and Magnuson). The daily and AM peak hour rates were estimated based on these results.

The baseline rates and equations applied for each land use type are summarized in Table 5. This analysis and report were prepared to support a 20 -year master planning process and the specific types and sizes of land uses could evolve in the future as the campus is re-developed, Table 5 is useful to provide context for how the MDP trip estimates were derived and to help future reviewers and the general public understand how future permit submittals might compare to the land uses and trip rates assumed herein.

As described in ITE's Trip Generation Handbook, ${ }^{23}$ "Trip Generation Manual contains no data on mode shares for baseline site trip generation. For this Handbook, a limited amount of weekday peak period (7:00-9:00 a.m., 4:00-6:00 p.m.) site trip generation mode share data were collected for baseline sites to provide a general starting point for baseline mode shares for the most common land use types. Baseline [mode share] data were collected at apartments, motels, offices, shopping centers, restaurants, a bank, and a bowling alley. The land use types were selected so the data would be transferrable to similar land uses (for example, residential apartment mode shares should be applicable to all suburban baseline apartment classifications). Tables B. 1 and B. 2 show the available weekday AM and PM peak period average mode shares and ranges for the baseline sites at which data were collected. There are not enough samples to derive precise percentages by mode for the land use codes for which data were collected.... Nearly half of the land use category averages in the tables are 100 percent motor vehicle."

Tables B. 1 and B. 2 in the Trip Generation Handbook only provides baseline mode-of-travel information for one of land uses being considered and evaluated in the MDP-General Office-and lists it with $1 \%$ transit for AM peak and $0 \%$ for PM peak. No baseline transit or non-auto data are provided for any of the other land uses. Therefore, as noted above the baseline trip generation rates and equations applied for the various site uses assumed that $99 \%$ to $100 \%$ of the trips would be by vehicular modes.

In the long-term, more of the site's employees are expected to use transit and non-automobile modes compared to the baseline suburban trip generation rates and equations. As noted previously, Sound Transit is constructing the Lynnwood Link Light Rail Extension with a new transit station located between NE $145^{\text {th }}$ and NE $148^{\text {th }}$ Streets, about a mile west of the Fircrest School Campus. Mode-of-travel estimates for the site's future employees were estimated based on a combination of sources. The 2021 five-year American Community Survey (ACS) data for workers (16 years and older) in Census tract \#211 (which includes the site) indicated about $10.4 \%$ commuted by transit and $2.3 \%$ walked or biked. These survey data do not account for enhancements in transit that will occur once Sound Transit's $145^{\text {th }}$ Street Station is complete. In addition, the estimates considered, the City of Shoreline's $145^{\text {th }}$ Street Station Subarea Plan, which was prepared for the surrounding area north of NE $145^{\text {th }}$ Street and extended to $15^{\text {th }}$ Avenue NE at the southwest corner of the Fircrest Campus. The City's plan anticipates $10 \%$ of external trips to and from the subarea would be by transit and $12 \%$ would be walking and biking (Table 7-2). Unfortunately, no information was provided in the City's plan related to the methodology used to derive those factors. However, based on these expectations, the proximity of the light rail station (about one mile away), transit operating adjacent to the site, the ACS survey results, and existing or anticipated future vicinity non-motorized facilities, it is reasonable to assume some non-auto employee trips for the Fircrest Campus by 2042. The analysis assumed a $6 \%$ non-auto (transit, walk and bike) adjustment (or 45 out of 752 unadjusted PM peak trips) from the baseline suburban ITE trip generation results-which is less than $30 \%$ of the level assumed in the City's $145^{\text {th }}$ Street Station Subarea Plan. Table 6 presents trip generation estimates for the existing Fircrest Campus (No Action) and year 2042 with the MDP; the estimated net change due to the MDP is also shown. The detailed trip generation calculations and adjustments are provided in Appendix C.

[^6]Fircrest School Master Development Plan
Updated Transportation Technical Report
Table 5. Trip Generation Rates \& Equations

| Land Use | ITE LU <br> Code | Equations ${ }^{\text {a }}$ Rates (in / out \%s) |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Daily | AM Peak Hour | PM Peak Hour |
| Assisted Living | 254 | 2.60 trips / bed 50\% / 50\% | $\begin{gathered} 0.18 \text { trips / bed } \\ 60 \% / 40 \% \end{gathered}$ | $\begin{gathered} 0.24 \text { trips / bed } \\ 39 \% / 61 \% \end{gathered}$ |
| Nursing Home | 620 | $\begin{gathered} 3.06 \text { trips / bed } \\ 50 \% / 50 \% \end{gathered}$ | $\begin{gathered} 0.14 \text { trips / bed } \\ 72 \% / 28 \% \\ \hline \end{gathered}$ | $\begin{gathered} 0.14 \text { trips / bed } \\ 33 \% ~ / ~ 67 \% \end{gathered}$ |
| Single-Tenant Office | 715 | $\begin{gathered} 13.07 \text { trips / 1,000 sfgfa } \\ 50 \% / 50 \% \end{gathered}$ | $\begin{gathered} \mathrm{T}=1.89(\mathrm{X})-7.67 \\ 89 \% / 11 \% \end{gathered}$ | $\begin{gathered} \mathrm{T}=1.72(\mathrm{X})+7.89 \\ 15 \% / 85 \% \end{gathered}$ |
| Daycare Center | 565 | $\begin{gathered} 47.62 \text { trips / 1,000 sfgfa } \\ 50 \% / 50 \% \\ \hline \end{gathered}$ | $\begin{gathered} 11.00 \text { trips / 1,000 sf } \\ 53 \% / 47 \% \\ \hline \end{gathered}$ | $\begin{gathered} 11.12 \text { trips / 1,000 sf } \\ 47 \% / 53 \% \\ \hline \end{gathered}$ |
| Hospital | 610 | $\begin{gathered} 10.77 \text { / 1,000 sfgfa } \\ 50 \% / 50 \% \\ \hline \end{gathered}$ | $\begin{gathered} \operatorname{Ln}(\mathrm{T})=0.60 \operatorname{Ln}(X)+2.52 \\ 67 \% / 33 \% \end{gathered}$ | $\begin{gathered} \operatorname{Ln}(T)=0.64 \operatorname{Ln}(X)+2.27 \\ 35 \% / 65 \% \end{gathered}$ |
| General Office | 710 | $\begin{gathered} \operatorname{Ln}(T)=0.87 \operatorname{Ln}(X)+3.05 \\ 50 \% / 50 \% \end{gathered}$ | $\begin{gathered} \operatorname{Ln}(\mathrm{T})=0.86 \operatorname{Ln}(X)+1.16 \\ 88 \% / 12 \% \end{gathered}$ | $\begin{gathered} \operatorname{Ln}(\mathrm{T})=0.83 \operatorname{Ln}(\mathrm{X})+1.29 \\ 17 \% / 83 \% \end{gathered}$ |
| Medical/ Dental Office | 720 | 36.00 trips / 1,000 sfgfa 50\% / 50\% | $\begin{gathered} \operatorname{Ln}(T)=0.90 \operatorname{Ln}(X)+1.34 \\ 79 \% / 21 \% \end{gathered}$ | $\begin{gathered} T=4.07(X)-3.17 \\ 30 \% / 70 \% \end{gathered}$ |
| Off-Leash Dog Area ${ }^{\text {b }}$ | N/A | 27.59 trips / acre <br> 50\% / 50\% | 2.76 trips / acre <br> 50\% / 50\% | $\begin{gathered} 2.76 \text { trips / acre } \\ 50 \% / 50 \% \end{gathered}$ |

Source: Institute of Transportation Engineers (ITE) Trip Generation, $11^{\text {th }}$ Edition, September 2021 (unless otherwise noted).
a. $\quad T=$ number of trips, $X=$ square feet gross floor area (sfgfa).
b. PM Peak hour rate from Transportation Impact Analysis for Off-Leash Dog Area(s) at the Chambers Creek Properties, Heffron

Transportation, Inc., Nov. 2006. Daily rate estimated as ten times the PM peak rate; AM rate estimated to be the same as PM rate.
Table 6. Trip Generation Summary - Fircrest Campus: No Action and With Master Plan

| Lane Uses / Sizes (assumes full occupancy) | ITE LU <br> Code | Daily <br> Trips | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | In | Out | Total | In | Out | Total |
| DSHS Fircrest School: No Action |  |  |  |  |  |  |  |  |
| Nursing Home - 120 beds | 620 | 350 | 12 | 4 | 16 | 6 | 10 | 16 |
| Assisted Living - 160 Beds | 254 | 390 | 16 | 11 | 27 | 14 | 22 | 36 |
| Single-Tenant Office - 89,958 sfgfa | 715 | 1,110 | 135 | 17 | 152 | 23 | 130 | 153 |
| Off-Leash Dog Area - 1.4 acres | N/A | 40 | 2 | 2 | 4 | 2 | 2 | 4 |
| Total for Fully Occupied Existing Uses |  | 1,890 | 165 | 34 | 199 | 45 | 164 | 209 |
| DSHS Fircrest School: Proposed Master Development Plan |  |  |  |  |  |  |  |  |
| Nursing Home - 120 beds | 620 | 350 | 12 | 4 | 16 | 5 | 11 | 16 |
| Single-Tenant Office - 89,958 sfgfa | 715 | 1,110 | 135 | 17 | 152 | 23 | 130 | 153 |
| Behavioral Health Hospital - 52,000 sfgfa (48 beds) | 610 | 530 | 84 | 41 | 125 | 40 | 74 | 114 |
| Assisted Living - 152 beds | 254 | 370 | 16 | 10 | 26 | 13 | 21 | 34 |
| General Office - 23,320 sfgfa | 710 | 310 | 40 | 5 | 45 | 8 | 39 | 47 |
| Day Care Center - 5,000 sfgfa | 565 | 110 | 14 | 12 | 26 | 12 | 14 | 26 |
| Medical/Dental Office - 85,000 sfgfa | 720 | 2,880 | 155 | 41 | 196 | 97 | 225 | 322 |
| Total for Retained and Proposed New Uses |  | 5,660 | 456 | 130 | 586 | 198 | 514 | 712 |
| Net Change With Master Development Plan |  | 3,770 | 291 | 96 | 387 | 153 | 350 | 503 |

Source: Heffron Transportation, Inc. using ITE's Trip Generation Manual (11 ${ }^{\text {th }}$ Ed, Sept. 2021) with 6\% non-auto trip reduction, Nov. 2023.

### 3.2.2. Trip Distribution and Assignment

Trip distribution patterns were developed based on a combination of resources including: 1) home-towork (and vice versa) trip data from OnTheMap ${ }^{24}$ for employees working in the site's Census tract; 2) Google Maps predictive travel-route and travel-time results; 3) traffic patterns at study-area intersections, and 4) the project's planned site access locations. The traffic estimates presented in Table 6 were assigned to the local roadway network. As noted in Section 3.1, "The new development at the southeast corner would be accessed from a new driveway on NE $150^{\text {th }}$ Street located about 290 feet west of $20^{\text {th }}$ Avenue NE. The eastern most driveway on NE $150^{\text {th }}$ Street would be removed." All vehicular access to the proposed new southeastern commercial development would be only from NE $150^{\text {th }}$ Street-the existing access connection through the campus to NE $155^{\text {th }}$ Street would be eliminated. As a result, the projectrelated increase in trips on NE $150^{\text {th }}$ Street is a result of both the concentration of new development that would all use that new driveway (over 113,000 sf of new professional office space, including the daycare center) and to a lesser extent the closure of the existing driveway to the east. Figure 6 shows the trip distribution patterns and net new trip assignments for AM and PM peak hours.

The AM and PM peak hour project trips were added to the forecast 2042 without-project traffic volumes for each period to represent future conditions with the Fircrest School MDP. Figure 7 shows the forecast 2042 with-project AM and PM peak hour traffic volumes.

[^7]


Figure 7
Fircrest School Master Plan Traffic Impact Statement

Forecast 2042-With-Project Traffic Volumes AM and PM Peak Hours

### 3.3. Traffic Operations

Levels of service for the study-area intersections were calculated using the 2042-with-project traffic volumes and the methodology described earlier in this report. Table 7 shows the results of the analysis; levels of service for the 2042 -without-project conditions are shown for comparison. The LOS calculation sheets are provided in Appendix B.

Table 7. Level of Service Summary - Forecast-2042-Without- \& With-Project Conditions

| Intersection Type / Location | AM Peak Hour |  |  |  |  |  | PM Peak Hour |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Without Project |  |  | With Project |  |  | Without Project |  |  | With Project |  |  |
| Signalized Intersections | LOS ${ }^{1}$ | Delay ${ }^{2}$ | v/c ${ }^{3}$ | LOS | Delay | v/c | LOS | Delay | v/c | LOS | Delay | v/c |
| 1. NE 155th St / $5^{\text {th }}$ Ave NE | C | 22.1 | 0.85 | C | 22.7 | 0.85 | C | 33.2 | 0.99 | D | 48.1 | 1.12 |
| 2. NE 155 ${ }^{\text {th }}$ St / $15^{\text {th }}$ Ave NE | C | 32.9 | 1.00 | D | 37.7 | 1.02 | D | 36.9 | 1.01 | E | 63.5 | 1.19 |
| 3. NE 150 ${ }^{\text {th }}$ St $/ 15^{\text {th }}$ Ave NE | B | 17.2 | 0.78 | C | 20.9 | 0.87 | B | 18.9 | 0.70 | D | 45.3 | 1.18 |
| All-Way-Stop Intersection | LOS | Delay | v/c | LOS | Delay | v/c | LOS | Delay | v/c |  |  |  |
| 4. NE $150^{\text {th }}$ St $/ 25^{\text {th }}$ Ave NE |  | 126.5 |  | F | 140.1 |  | F | 83.2 |  | F | 94.5 |  |
| Northbound Movements | E | 39.8 | 0.92 | F | 52.7 | 1.04 | F | 137.7 | 1.22 | F | 158.2 | 1.27 |
| Eastbound Left Turns | F | 143.9 | 1.32 | F | 165.4 | 1.37 | C | 24.7 | 0.75 | D | 28.7 | 0.82 |
| Westbound Left Turns | C | 19.5 | 0.42 | C | 20.6 | 0.44 | B | 11.8 | 0.07 | B | 12.0 | 0.07 |
| Southbound Movements | F | 182.8 | 1.41 | F | 197.1 | 1.47 | B | 14.3 | 0.44 | B | 14.7 | 0.45 |
| Stop Controlled Intersection | LOS | Delay | v/c | LOS | Delay | v/c | LOS | Delay | v/c |  |  |  |
| 5. NE $150^{\text {th }}$ St / $20^{\text {th }}$ Ave NE | A | 2.6 |  | A | 1.8 |  | A | 4.3 |  | A | 3.5 |  |
| Northbound Movements | C | 19.0 | 0.23 | C | 18.1 | 0.24 | B | 14.1 | 0.31 | B | 14.4 | 0.32 |
| Eastbound Left Turns | A | 8.1 | 0.01 |  | n/a ${ }^{4}$ |  | A | 7.6 | 0.00 |  | n/a ${ }^{4}$ |  |
| Westbound Left Turns | A | 8.4 | 0.03 | A | 8.5 | 0.03 | A | 8.0 | 0.01 | A | 8.1 | 0.01 |
| Southbound Movements | C | 22.0 | 0.15 |  | $n / \mathrm{a}^{4}$ |  | B | 12.8 | 0.09 |  | n/a ${ }^{4}$ |  |
| 6. NE 150 ${ }^{\text {th }}$ St / New Access |  | $n / a^{5}$ |  | A | 3.0 |  |  | $n / a^{5}$ |  | A | 5.4 |  |
| Eastbound Left Turns |  |  |  | A | 9.5 | 0.27 |  |  |  | A | 8.1 | 0.10 |
| Southbound Movements |  |  |  | C | 17.0 | 0.17 |  |  |  | C | 15.1 | 0.46 |

Source: Heffron Transportation, Inc., May 2022.

1. LOS = Level of service. LOS E shaded $\square$ LOS F shaded $\square$;
2. Delay = Average delay per vehicle in seconds.
3. $\quad v / c=$ Volume-to-capacity ratio.
4. $n / a=$ not applicable, movement eliminated with removal of north leg of intersection with project.
5. $n / a=$ not applicable, driveway would not exist without project.

As shown, the additional traffic generated by Fircrest School campus with the MDP is forecast to add delay to each of the signalized study-area intersections during both peak periods. Based on the level of delay forecast to be added and the City of Shoreline's currently-adopted LOS standards, it may be desirable to implement operational mitigation measures at the main access intersection on $15^{\text {th }}$ Avenue NE at NE $155^{\text {th }}$ Street. Signal phasing and channelization changes (to provide concurrent protectedpermitted left-turn phasing) could reduce delays noticeably (to 48.7 seconds per vehicle). It may be appropriate for the project to contribute a proportionate share toward the costs of signal and channelization improvements to mitigate these impacts. Project traffic is estimated to represent up to $11 \%$ of the total entering peak hour volumes and would be a reasonable contribution portion, if these improvements are not incorporated into the City's Transportation Impact Fee system. It is noted that, at
the time of this report, these locations have not been identified as growth projects for inclusion in the City's TIF project list.

The NE $150^{\text {th }}$ Street $/ 25^{\text {th }}$ Avenue NE intersection, which is an all-way stop, is forecast to operate at LOS F without the project and the relatively small number of added AM and PM peak hour project trips are forecast to cause large increases in delay. As a result, it would also be appropriate for the project to contribute a proportionate share toward the costs of operational improvements (such as signalization or conversion to a roundabout) to mitigate these impacts. Project traffic is estimated to represent between $2.7 \%$ and $3.4 \%$ of the total entering AM and PM peak hour volumes and would be reasonable contribution portions, if the improvement is not incorporated into the City's Transportation Impact Fee system. The city has identified this location as a growth project, but has not yet updated its TIF projects list.

### 3.4. Traffic Safety

The new and expanded development contemplated by the MDP could increase traffic at the study-are intersections and statistically, the number of collisions could increase as traffic increases. However, the project does not include any substantial changes to the roadway network that are expected to result in new adverse safety concerns. The collision data provided for the study-area intersections do not indicate any unusual existing safety conditions that would impact or be impacted by the proposed project and the proposed project is not expected to adversely affect the safety in the area.

### 3.5. Site Access Evaluation

The existing campus has two access points-one main signalized access on $15^{\text {th }}$ Avenue NE opposite NE $155^{\text {th }}$ Street, and one on NE $150^{\text {th }}$ Street opposite $20^{\text {th }}$ Avenue NW. The main campus access would remain from on $15^{\text {th }}$ Avenue NE. The new development at the southeast corner would be accessed from a new driveway on NE $150^{\text {th }}$ Street located about 290 feet west of $20^{\text {th }}$ Avenue NE, while the eastern most driveway on NE $150^{\text {th }}$ Street would be removed. The existing gated access on $15^{\text {th }}$ Avenue NE about 350 feet north of NE $155^{\text {th }}$ Street is planned to be retained, but remain gated with access limited to emergency and/or maintenance vehicles.

The proposed new access on NE $150^{\text {th }}$ Street would meet the minimum clearance from other intersections (greater than 75 feet for access points on a Collector Arterial). It would also meet the minimum spacing for access driveways on the north side of the street; however, because there are driveways serving singlefamily residential lots on the south side of the street, the access location may require approval for reduced spacing from the City's Engineering Director.

NE $150^{\text {th }}$ Street has crest vertical curves to the west and east of the planned site access locations. Sight distance to and from this access location is clear for more than 500 feet in both directions and would meet the recommended level for a stop-controlled minor approach as outlined in Table 13 of the City's 2023 Engineering Development Manual ${ }^{25}$ ( 335 feet for an intersection with a major roadway with a posted speed limit of 30 mph ). However, there is currently a rockery, vegetation, and trees located behind the sidewalk at the anticipated access locations. At the time of site development, additional review will be required to ensure that the applicable sight distance triangles would be provided.

The operational analyses of the planned new site access location on NE $150^{\text {th }}$ Street was presented previously. It is forecast to operate at LOS A overall with all movements operating at LOS C or better during AM and PM peak hour conditions. The HCM 6 LOS calculation includes estimates of the $95^{\text {th }}$ percentile queues, which are reported to be about one vehicle for eastbound left-turns into the site during both peak periods. The $95^{\text {th }}$-percentile queues for vehicles leaving the access driveway onto NE $150^{\text {th }}$ Street are reported to be less than three vehicles during both peak periods.

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### 3.6. Parking Supply \& Demand

Due to the unique nature and variety of uses on the Fircrest School Campus parking demand is largely attributed to the number of full time equivalent (FTE) employees on duty and the number of residents at the campus. The existing campus currently has 541 parking spaces spread throughout the campus with larger clusters of parking near the Activities Building, Kitchen, Administration Building, and the Pat ' N '/ ' Y ' Buildings. With the proposed MDP, the total number of parking spaces is anticipated to increase to 830 spaces (an increase of 289 spaces compared to existing conditions). This supply is expected to exceed the parking demand for the campus which is estimated to total 751 vehicles. ${ }^{26}$ Table 8 shows the parking supply, estimated demand for each building on campus, and the proposed parking supply standards.

Table 8. Fircrest School Campus Proposed Parking Supply and Demand Summary

| Building | Parking Supply | Peak <br> Parking <br> Demand | Proposed Parking Spaces Standard |
| :---: | :---: | :---: | :---: |
| Existing Buildings to Remain |  |  |  |
| 16-Bed ICF/ID Cottages | 40 | 80 | 1 per 5 residents, plus 1 per FTE employee on duty |
| Activities Building | 30 | 8 | 1 per FTE employee on duty +3 spaces for deliveries/visitors |
| Administration Building | 24 | 53 | 1 per FTE employee on duty +3 spaces for deliveries/visitors |
| Kitchen | 53 | 23 | 1 per FTE employee on duty +3 spaces for deliveries/visitors |
| Chapel | 46 | 27 | 1 per 5 fixed seats +1 per 50 square feet of gross floor area without fixed seats used for assembly purposes a |
| Existing Parking Spaces Total | 193 | 191 |  |
| Near-Term Developments (estimated completion by 2030) |  |  |  |
| 120-Bed Nursing Facility | 130 | 101 | Nursing Facility: 1 per 5 residents, plus 1 per FTE employee on duty <br> Laundry: 1 per FTE employee on duty +1 loading space |
| Adult Training Program (Relocation) | 14 | 38 | 1 per FTE employee on duty +3 spaces for deliveries/visitors |
| 48-Bed Behavioral Health Facility | 89 | 31 | 1 per 8 residents, plus 1 per FTE employee on duty |
| South Building - Professional Office/Daycare | 81 | 51 | Professional office uses: 1 per 500 square feet Daycare II: $2+1$ for each 20 clients ${ }^{\text {b }}$ |
| Near-Term Parking Spaces Total | 314 | 221 |  |
| Long-Term Developments (estimated completion by 2040) |  |  |  |
| Maintenance Facility | 20 | 60 | 1 per FTE employee on duty + 10 loading space |
| Commissary Building | 15 | 6 | 1 per FTE employee on duty + 2 spaces for deliveries/visitors |
| 4-Bedroom ICF/ID Cottages | 75 | 96 | 1 per 5 residents, plus 1 per FTE employee on duty |
| North Building - Professional Office | 193 | 170 | 1 per 500 square feet |
| Recreation Space | 20 | 7 | 10 per acre |
| Long-Term Parking Spaces Total | 323 | 339 |  |
| Total Campus (All Development) | 830 | 751 |  |

Source: AHBL, November 2023.
a. Assume 100 seats and $10 \%$ of the chapel is without seats
b. Assumes 5,000 sf of Daycare with up to 40 clients

[^8]In total the parking supply on campus in the MDP exceeds the parking demand by approximately 79 spaces. Some of the buildings on campus have fewer parking spaces than the demand stipulated for the proposed use, however other nearby buildings have an excess parking supply. Most buildings on the campus are in close proximity to one another and to multiple parking areas allowing for additional parking spaces to be available when needed. For example, the 16-bed ICF Cottages have a parking demand of 80 spaces and parking supply of 40 spaces, however, the northern ICF Cottages are adjacent to the kitchen and new Behavioral Health Facility which both have an excess parking supply.

It is noted that the total peak parking demand for the cumulative uses reflects a worst-case condition that assumes all of the uses have their peak demand at the same time of day. In reality, peak demand times could occur at different times of day. For example, office uses typically have peak demand times in the mid-morning or mid-afternoon, while the nursing facilities are likely to have their peak demand early in the morning during the shift change. Therefore, peak cumulative demand would likely be less than reported in Table 8.

Parking supply for the individual masterplan elements would be determined at the time of permit application, and the number of spaces needed will depend on the intended building program. It is expected that sufficient supply would be provided to meet project parking demand. If future demand is estimated to exceed the supply, then the proponent should be required to perform further studies to determine if parking mitigation would be needed, which could include sharing parking with other uses on site or in the vicinity, implementing trip and parking demand reduction strategies, or other measures.

### 3.7. Transit

Some transit trips are expected to be generated by employees working at the site. Based on the trip generation estimates presented previously and the $6 \%$ adjustment for non-auto modes of travel, the campus could generate increases of up 360 transit trips per day with about 35 in the AM peak hour and 45 in the PM peak hour. Due to the proximity to local bus stops and access to future light rail (the nearest bus stops are located at the NE $155^{\text {th }}$ Street $/ 15^{\text {th }}$ Avenue NE intersection), the estimated additional transit trips are not expected to result in adverse impacts to transit facilities or service.

### 3.8. Non-Motorized Transportation Facilities

Fircrest School campus would continue to generate pedestrian and bicycle trips within the site vicinity. The increase in employment is expected to proportionally increase the number of pedestrian and bicycle trips generated at the site. As noted, frontage improvements (including new sidewalk) would be constructed along the portions of campus included in the MDP in phases with triggers based on campus improvements. These improvements would enhance the non-motorized environment for the site and the project is not expected to adversely affect non-motorized transportation facilities.

The City of Shoreline's 2024 to 2029 TIP and 2023 CIP Map show that the City intends to repair and replace sidewalks along $15^{\text {th }}$ Avenue NE between NE $155^{\text {th }}$ Street and NE $175^{\text {th }}$ Street, with construction planned in 2023. According to City staff, this planned project is focused primarily on repairing existing sidewalks located on the west side of $15^{\text {th }}$ Avenue NE. There is also a conceptual plan for sidewalk along the east side of $15^{\text {th }}$ Avenue NE identified for potential construction in 2028, but that plan does not address the bike facility along the frontage of the Fircrest campus site. ${ }^{27}$ It is noted that the Fircrest School MDP area fronts $15^{\text {th }}$ Avenue NE north of NE $155^{\text {th }}$ Street, but not south of NE $155^{\text {th }}$ Street. Development of the site requiring frontage improvements is likely many years in the future, and may occur after the City's sidewalk project. Remaining frontage improvement needs would be coordinated with the City.

[^9]
## 4. RECOMMENDATIONS / CONCLUSIONS

Based on the above findings, the following measures would be incorporated into the project proposal and/or are recommended to minimize the traffic and parking impacts associated with the Fircrest MDP project.
A. Construction Transportation Management Plan (CTMP) - DSHS should require the selected contractor to develop a CTMP. The CTMP should address traffic and pedestrian control during each major phase of construction. It should confirm truck routes, lane closures, walkway routes and closures, and parking disruptions, as necessary. The CTMP may also include measures to keep adjacent streets clean on a daily basis at the truck exit points (such as street sweeping or on-site truck wheel cleaning) to reduce tracking dirt off site. The CTMP should identify parking locations for the construction personnel, staff, and fleet vehicles.
B. Travel Demand Management Plan (TDMP) - A TDMP is a standard requirement for MDPs in the City of Shoreline. The TDMP for the Fircrest Campus would evolve as the individual elements are implemented and as owner/operators are identified. The TDMP would be based on the current Commute Trip Reduction (CTR) Program that is already in place for the Fircrest campus and includes the following elements:

- Long-term bike storage spaces for employee use throughout the campus;
- Lockers and shower facilities for those who walk or ride to and from the site;
- Transit fare reimbursement (currently $\$ 65$ per month) for DSHS employees who commute via public transportation;
- Rideshare, carpool, and vanpool ride matching support;
- Guaranteed ride home for employees who carpool, or take transit to work;
- Flexible employee work schedules (e.g., 4-day workweeks, etc.);
- Hybrid and/or telecommuting options for eligible employees; and
- An Employee Transportation Coordinator to assist employees with finding alternatives to driving alone and other information about commute alternatives.

The TDMP would be monitored through the existing annual reporting requirements of the CTR Program, which beginning in 2023, provides performance reports to the City of Shoreline.
C. Contribute to cost of improvements (e.g., signalization or conversion to roundabout) at NE $\mathbf{1 5 0}^{\text {th }}$ Street $/ \mathbf{2 5}^{\text {th }}$ Avenue NE - The NE $150^{\text {th }}$ Street $/ 25^{\text {th }}$ Avenue NE intersection is forecast to operate at LOS F without the project. The added AM and PM peak hour project trips are forecast to cause large increases in delay. As a result, it would also be appropriate for the project to contribute a proportionate share toward the costs of operational improvements (such as signalization or conversion to roundabout) to mitigate these impacts. Project traffic is estimated to represent between $2.7 \%$ and $3.4 \%$ of the total entering AM and PM peak hour volumes and would be reasonable contribution portions, if the improvement is not incorporated into the City's Transportation Impact Fee system. The city has identified this location as a growth project, but has not yet updated the TIF projects list.
D. Signal optimization for NE $\mathbf{1 5 5}^{\text {th }}$ Street $/ \mathbf{1 5}^{\text {th }}$ Avenue NE intersection - Based on the level of delay forecast to be added and the City of Shoreline's currently-adopted LOS standards, it may be desirable to implement operational mitigation measures at the signalized NE $155^{\text {th }}$ Street $/ 15^{\text {th }}$ Avenue NE intersection. Signal phasing and channelization changes at the NE $155^{\text {th }}$ Street intersection (to provide concurrent protected-permitted left-turn phasing) could reduce delays noticeably. It may be appropriate for the project to contribute a proportionate share toward the costs of signal optimization improvements to mitigate these impacts. Project traffic is estimated to
represent up to $11 \%$ of the total entering peak hour traffic at the NE $155^{\text {th }}$ Street intersection, which would be reasonable contribution portion, if these improvements are not incorporated into the City's Transportation Impact Fee system. At the time of this report, this location has not been identified as a growth project for inclusion in the City's TIF project list.
E. Parking analysis at time of development permitting - Parking supply for each individual MDP element would be determined at the time of permit application, and the number of spaces needed will depend on the intended building program. It is expected that sufficient supply would be provided to meet project parking demand. If future demand is estimated to exceed the supply, then the proponent should be required to perform further studies to determine if parking mitigation (e.g., share parking or trip reduction strategies) would be needed.

In addition to the recommended measures above, the City of Shoreline collects Transportation Impact Fees (TIFs) from applicants seeking building permits for either new developments or changes of use. The impact fee rate currently in effect (2023) is $\$ 9,271.05$ per new PM peak hour vehicle trip. The City has also identified fee rates for some select relevant land uses-Assisted living $\$ 842.03$ / bed; Hospital: $\$ 11.05$ / sf; Medical offices: $\$ 30.17$ / sf; General office: $\$ 16.60$ / sf; and Daycare center: $\$ 45.04$ / sf.

Based on the estimated change to trip-generating DSHS program elements, only the new Behavioral Health Hospital is expected to increase trips and those would be offset by the reduction in ICF/ID cottage beds ( 8 fewer assisted-living beds) and the removal of the off-leash dog area. The new commercial development element on the south portion of the campus would be entirely new for the purposes of TIFs.

Based on the above, the potential TIF for all contemplated MDP uses could range from about $\$ 3,891,920$ ( $\$ 715,160$ for DSHS Program elements and $\$ 3,176,760$ for other commercial elements) to $\$ 4,663,340$ ( $\$ 1,001,275$ for DSHS Program elements and $\$ 3,662,065$ for other commercial elements). These estimates are based on the currently adopted fee rates and depend on whether the per-trip fee rate or rates for specific land uses are applied. It is important to note that impact fees are assessed at the time of building permit issuance and at the rates in place at that time. Increases in the fee rates are calculated annually (by January $1^{\text {st }}$ ) and typically based on the Seattle-Tacoma-Bellevue Consumer Price Index for all urban consumers (CPI-U). In addition, the City is currently in the process of updating its TIF calculations and project lists. Fees will be assessed with each permit based on how many trips that portion of the overall MPD project adds and new TIF calculations will be required with each permit application. Individual building permit applications will reference this MDP for any agreed upon reductions.

## APPENDIX A Level of Service Definitions

Levels of service (LOS) are qualitative descriptions of traffic operating conditions. These levels of service are designated with letters ranging from LOS A, which is indicative of good operating conditions with little or no delay, to LOS F, which is indicative of stop-and-go conditions with frequent and lengthy delays. Levels of service for this analysis were developed using procedures presented in the Highway Capacity Manual, $6^{\text {th }}$ Edition (Transportation Research Board, 2016).

Level of service for signalized intersections is defined in terms of delay. Delay can be a cause of driver discomfort, frustration, inefficient fuel consumption, and lost travel time. Specifically, level-of-service criteria are stated in terms of the average delay per vehicle in seconds. Delay is a complex measure and is dependent on a number of variables including: the quality of progression, cycle length, green ratio, and a volume-to-capacity ratio for the lane group or approach in question. Table A-1 shows the level of service criteria for signalized intersections from the Highway Capacity Manual, $6^{\text {th }}$ Edition.

Table A-1. Level of Service for Signalized Intersections

| Level of Service | Average Delay Per Vehicle | General Description |
| :---: | :---: | :--- |
| A | Less than 10.0 Seconds | Free flow |
| B | 10.1 to 20.0 seconds | Stable flow (slight delays) |
| C | 20.1 to 35.0 seconds | Stable flow (acceptable delays) |
| D | 35.1 to 55.0 seconds | Approaching unstable flow (tolerable <br> delay-occasionally wait through more <br> than one signal cycle before |
|  |  | proceeding. |
| E | 55.1 to 80.0 seconds | Unstable flow (approaching capacity) |
| F | Greater than 80.0 seconds | Forced flow (jammed) |

Source: Transportation Research Board, Highway Capacity Manual, 2016.
For unsignalized intersections, level of service is based on the average delay per vehicle for each turning movement. The level of service for a two-way, stop-controlled intersection is determined by the computed or measured control delay and is defined for each minor movement. Delay is related to the availability of gaps in the main street's traffic flow, and the ability of a driver to enter or pass through those gaps. Table A-2 shows the level of service criteria for unsignalized intersections from the Highway Capacity Manual, $6^{\text {th }}$ Edition.

Table A-2. Level of Service Criteria for Unsignalized Intersections

| Level of Service | Average Delay <br> (seconds per vehicle) |
| :---: | :---: |
| A | Less than 10.0 |
| B | 10.1 to 15.0 |
| C | 15.1 to 25.0 |
| D | 25.1 to 35.0 |
| E | 35.1 to 50.0 |
| F | Greater than 50.0 |

Source: Transportation Research Board, Highway Capacity Manual, 2016.

## APPENDIX B LOS Calculation Sheets

|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


| Lane Group | EBL | $\rightarrow$ |  | WBL | $\leftarrow$ WBT |  | 4 | 4 NBT | NBR |  | ¢ SBT | ¢ SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Actuated g/C Ratio |  | 0.08 |  |  | 0.15 |  | 0.59 | 0.59 |  | 0.68 | 0.68 |  |
| $\mathrm{v} / \mathrm{C}$ Ratio |  | 0.06 |  |  | 0.77 |  | 0.01 | 0.21 |  | 0.22 | 0.37 |  |
| Control Delay |  | 36.2 |  |  | 44.3 |  | 17.5 | 12.2 |  | 13.4 | 12.2 |  |
| Queue Delay |  | 0.0 |  |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay |  | 36.2 |  |  | 44.3 |  | 17.5 | 12.2 |  | 13.4 | 12.2 |  |
| LOS |  | D |  |  | D |  | B | B |  | B | B |  |
| Approach Delay |  | 36.3 |  |  | 44.3 |  |  | 12.2 |  |  | 12.4 |  |
| Approach LOS |  | D |  |  | D |  |  | B |  |  | B |  |
| Queue Length 50th (ft) |  | 3 |  |  | 100 |  | 1 | 45 |  | 24 | 84 |  |
| Queue Length 95th (ft) |  | 17 |  |  | 177 |  | 6 | 129 |  | 121 | 328 |  |
| Internal Link Dist (ft) |  | 20 |  |  | 1243 |  |  | 592 |  |  | 360 |  |
| Turn Bay Length (ft) |  |  |  |  |  |  | 45 |  |  | 80 |  |  |
| Base Capacity (vph) |  | 309 |  |  | 388 |  | 350 | 1913 |  | 689 | 2290 |  |
| Starvation Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio |  | 0.03 |  |  | 0.60 |  | 0.01 | 0.21 |  | 0.22 | 0.37 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type: Other
Cycle Length: 110
Actuated Cycle Length: 110
Offset: 14 (13\%), Referenced to phase 2:SBTL and 6:NBTL, Start of Green
Natural Cycle: 90
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 0.77
Intersection Signal Delay: 16.9
Intersection LOS: B
Intersection Capacity Utilization 59.7\%
ICU Level of Service B
Analysis Period (min) 15

Splits and Phases: 1: 15th Ave NE \& NE 150th St


| Lane Group | FBL | $\rightarrow$ | EBR | WBL |  |  | 4 | ¢ ${ }_{\text {NBT }}$ | $\stackrel{+}{\text { NBR }}$ |  | ¢ SBT | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | $\uparrow$ | \% |  | $\uparrow$ | \% | \% | $\hat{\beta}$ |  | ${ }^{7}$ | $\uparrow$ | 7 |
| Traffic Volume (vph) | 59 | 24 | 281 | 4 |  | 7 | 184 | 228 | 20 | 54 | 693 | 253 |
| Future Volume (vph) | 59 | 24 | 281 | 4 | 5 | 7 | 184 | 228 | 20 | 54 | 693 | 253 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 10 | 12 | 10 | 10 | 11 | 11 | 11 | 12 | 10 | 11 | 11 | 12 |
| Storage Length (ft) | 0 |  | 75 | 0 |  | 0 | 60 |  | 0 | 90 |  | 140 |
| Storage Lanes | 0 |  | 1 | 0 |  | 1 | 1 |  | 0 | 1 |  | 1 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  | 1.00 | 0.97 |  | 1.00 | 0.97 | 1.00 | 1.00 |  | 1.00 |  | 0.97 |
| Frt |  |  | 0.850 |  |  | 0.850 |  | 0.988 |  |  |  | 0.850 |
| Flt Protected |  | 0.966 |  |  | 0.978 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1799 | 1478 | 0 | 1244 | 994 | 1662 | 1784 | 0 | 1711 | 1801 | 1583 |
| Flt Permitted |  | 0.786 |  |  | 0.908 |  | 0.258 |  |  | 0.511 |  |  |
| Satd. Flow (perm) | 0 | 1460 | 1438 | 0 | 1154 | 968 | 450 | 1784 | 0 | 919 | 1801 | 1530 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  | 299 |  |  | 145 |  | 7 |  |  |  | 193 |
| Link Speed (mph) |  | 30 |  |  | 25 |  |  | 35 |  |  | 35 |  |
| Link Distance (ft) |  | 577 |  |  | 127 |  |  | 874 |  |  | 1332 |  |
| Travel Time (s) |  | 13.1 |  |  | 3.5 |  |  | 17.0 |  |  | 25.9 |  |
| Confl. Peds. (\#/hr) | 2 |  | 1 | 1 |  | 2 | 5 |  | 1 | 1 |  | 5 |
| Confl. Bikes (\#/hr) |  |  | 3 |  |  | 1 |  |  |  |  |  | 2 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 100\% | 0\% | 57\% | 5\% | 5\% | 5\% | 2\% | 2\% | 2\% |
| Adj. Flow (vph) | 63 | 26 | 299 | 4 | 5 | 7 | 196 | 243 | 21 | 57 | 737 | 269 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 89 | 299 | 0 | 9 | 7 | 196 | 264 | 0 | 57 | 737 | 269 |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | pm+pt | NA |  | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 4 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  | 4 | 4 |  | 4 | 2 |  |  | 6 |  | 6 |
| Detector Phase | 4 | 4 | 4 | 4 | 4 | 4 | 5 | 2 |  | 1 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 | 5.0 | 10.0 |  | 5.0 | 10.0 | 10.0 |
| Minimum Split (s) | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 12.0 | 21.0 |  | 12.0 | 23.0 | 23.0 |
| Total Split (s) | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 15.0 | 53.0 |  | 12.0 | 50.0 | 50.0 |
| Total Split (\%) | 27.8\% | 27.8\% | 27.8\% | 27.8\% | 27.8\% | 27.8\% | 16.7\% | 58.9\% |  | 13.3\% | 55.6\% | 55.6\% |
| Maximum Green (s) | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 | 10.0 | 48.0 |  | 7.0 | 45.0 | 45.0 |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) |  | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 |
| Lead/Lag |  |  |  |  |  |  | Lag | Lag |  | Lead | Lead | Lead |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes |  | Yes | Yes | Yes |
| Vehicle Extension (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 |
| Recall Mode | None | None | None | None | None | None | None | C-Max |  | None | C-Max | C-Max |
| Walk Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 |  |  | 7.0 | 7.0 |
| Flash Dont Walk (s) | 13.0 | 13.0 | 13.0 | 13.0 | 13.0 | 13.0 |  | 9.0 |  |  | 11.0 | 11.0 |
| Pedestrian Calls (\#/hr) | 2 | 2 | 2 | 2 | 2 | 2 |  | 0 |  |  | 5 | 5 |



Area Type: Other
Cycle Length: 90
Actuated Cycle Length: 90
Offset: $0(0 \%)$, Referenced to phase 2:NBTL and 6:SBTL, Start of Green
Natural Cycle: 75
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 0.75
Intersection Signal Delay: 16.2
Intersection Capacity Utilization 79.3\%
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 2: 15th Ave NE \& NE 155th St


| Lane Group | * | $\begin{aligned} & \rightarrow \\ & \text { EBT } \end{aligned}$ | EBR | WBL | $*$ WBT | 4 WBR | NBL | $\uparrow$ NBT | NBR | + | ¢ SBT | $\downarrow$ SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ |  | ${ }^{7}$ | $\uparrow$ |  | ${ }^{7}$ | $\uparrow$ |  | ${ }^{7}$ | $\uparrow$ |  |
| Traffic Volume (vph) | 47 | 195 | 56 | 140 | 407 | 22 | 90 | 52 | 26 | 63 | 393 | 168 |
| Future Volume (vph) | 47 | 195 | 56 | 140 | 407 | 22 | 90 | 52 | 26 | 63 | 393 | 168 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 11 | 11 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Storage Length (ft) | 110 |  | 0 | 100 |  | 0 | 105 |  | 0 | 160 |  | 0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | 1.00 | 0.99 |  | 1.00 | 1.00 |  | 1.00 |  |  |  | 0.99 |  |
| Frt |  | 0.966 |  |  | 0.992 |  |  | 0.951 |  |  | 0.955 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1703 | 1664 | 0 | 1736 | 1810 | 0 | 1703 | 1705 | 0 | 1687 | 1684 | 0 |
| Flt Permitted | 0.353 |  |  | 0.596 |  |  | 0.264 |  |  | 0.704 |  |  |
| Satd. Flow (perm) | 631 | 1664 | 0 | 1085 | 1810 | 0 | 473 | 1705 | 0 | 1250 | 1684 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 30 |  |  | 6 |  |  | 27 |  |  | 50 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 572 |  |  | 796 |  |  | 673 |  |  | 531 |  |
| Travel Time (s) |  | 13.0 |  |  | 18.1 |  |  | 15.3 |  |  | 12.1 |  |
| Confl. Peds. (\#/hr) | 5 |  | 4 | 4 |  | 5 | 2 |  |  |  |  | 2 |
| Confl. Bikes (\#/hr) |  |  | 1 |  |  | 1 |  |  |  |  |  | 1 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles (\%) | 6\% | 6\% | 6\% | 4\% | 4\% | 4\% | 6\% | 6\% | 6\% | 7\% | 7\% | 7\% |
| Adj. Flow (vph) | 49 | 205 | 59 | 147 | 428 | 23 | 95 | 55 | 27 | 66 | 414 | 177 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 49 | 264 | 0 | 147 | 451 | 0 | 95 | 82 | 0 | 66 | 591 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 2 |  |  | 2 |  |  | 4 |  |  | 4 |  |
| Permitted Phases | 2 |  |  | 2 |  |  | 4 |  |  | 4 |  |  |
| Detector Phase | 2 | 2 |  | 2 | 2 |  | 4 | 4 |  | 4 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Minimum Split (s) | 24.0 | 24.0 |  | 24.0 | 24.0 |  | 24.0 | 24.0 |  | 24.0 | 24.0 |  |
| Total Split (s) | 26.0 | 26.0 |  | 26.0 | 26.0 |  | 29.0 | 29.0 |  | 29.0 | 29.0 |  |
| Total Split (\%) | 47.3\% | 47.3\% |  | 47.3\% | 47.3\% |  | 52.7\% | 52.7\% |  | 52.7\% | 52.7\% |  |
| Maximum Green (s) | 21.0 | 21.0 |  | 21.0 | 21.0 |  | 24.0 | 24.0 |  | 24.0 | 24.0 |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Recall Mode | None | None |  | None | None |  | None | None |  | None | None |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 12.0 | 12.0 |  | 12.0 | 12.0 |  | 12.0 | 12.0 |  | 12.0 | 12.0 |  |
| Pedestrian Calls (\#/hr) | 5 | 5 |  | 5 | 5 |  | 7 | 7 |  | 7 | 7 |  |
| Act Effct Green (s) | 15.9 | 15.9 |  | 15.9 | 15.9 |  | 19.1 | 19.1 |  | 19.1 | 19.1 |  |


| Lane Group | ¢ EBL | $\rightarrow$ | EBR | WBL | $\leftarrow$ WBT |  | 4 NBL | ¢ ${ }_{\text {NBT }}$ | NBR | ¢ SBL | ¢ SBT | $\stackrel{\downarrow}{\text { SBR }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Actuated g/C Ratio | 0.35 | 0.35 |  | 0.35 | 0.35 |  | 0.42 | 0.42 |  | 0.42 | 0.42 |  |
| v/c Ratio | 0.22 | 0.44 |  | 0.39 | 0.71 |  | 0.48 | 0.11 |  | 0.13 | 0.81 |  |
| Control Delay | 14.5 | 13.4 |  | 15.7 | 20.5 |  | 20.7 | 7.1 |  | 9.7 | 22.1 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 14.5 | 13.4 |  | 15.7 | 20.5 |  | 20.7 | 7.1 |  | 9.7 | 22.1 |  |
| LOS | B | B |  | B | C |  | C | A |  | A | C |  |
| Approach Delay |  | 13.6 |  |  | 19.3 |  |  | 14.4 |  |  | 20.9 |  |
| Approach LOS |  | B |  |  | B |  |  | B |  |  | C |  |
| Queue Length 50th (ft) | 10 | 51 |  | 32 | 110 |  | 19 | 9 |  | 11 | 127 |  |
| Queue Length 95th (ft) | 31 | 104 |  | 72 | 200 |  | 62 | 30 |  | 31 | \#305 |  |
| Internal Link Dist (ft) |  | 492 |  |  | 716 |  |  | 593 |  |  | 451 |  |
| Turn Bay Length (t) | 110 |  |  | 100 |  |  | 105 |  |  | 160 |  |  |
| Base Capacity (vph) | 310 | 833 |  | 533 | 892 |  | 265 | 969 |  | 702 | 968 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn |  | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.16 | 0.32 |  | 0.28 | 0.51 |  | 0.36 | 0.08 |  | 0.09 | 0.61 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type: Other

Cycle Length: 55
Actuated Cycle Length: 45.7
Natural Cycle: 55
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.81
Intersection Signal Delay: 18.4
Intersection LOS: B
Intersection Capacity Utilization 79.6\% ICU Level of Service D
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 3: 5th Ave NE \& NE 155th St


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 47.5 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS | E |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 146 | 21 | 70 | 31 | 44 | 13 | 43 | 118 | 1 | 3 | 295 | 148 |
| Future Vol, veh/h | 146 | 21 | 70 | 31 | 44 | 13 | 43 | 118 | 1 | 3 | 295 | 148 |
| Peak Hour Factor | 0.64 | 0.64 | 0.64 | 0.63 | 0.63 | 0.63 | 0.63 | 0.63 | 0.63 | 0.73 | 0.73 | 0.73 |
| Heavy Vehicles, \% | 1 | 1 | 1 | 5 | 5 | 5 | 0 | 0 | 0 | 1 | 1 | 1 |
| Mvmt Flow | 228 | 33 | 109 | 49 | 70 | 21 | 68 | 187 | 2 | 4 | 404 | 203 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 25.6 |  |  | 14.6 |  |  | 17.7 |  |  | 80.8 |  |  |
| HCM LOS | D |  |  | B |  |  | C |  |  | F |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $27 \%$ | $62 \%$ | $35 \%$ | $1 \%$ |
| Vol Thru, \% | $73 \%$ | $9 \%$ | $50 \%$ | $66 \%$ |
| Vol Right, \% | $1 \%$ | $30 \%$ | $15 \%$ | $33 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 162 | 237 | 88 | 446 |
| LT Vol | 43 | 146 | 31 | 3 |
| Through Vol | 118 | 21 | 44 | 295 |
| RT Vol | 1 | 70 | 13 | 148 |
| Lane Flow Rate | 257 | 370 | 140 | 611 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.509 | 0.706 | 0.303 | 1.065 |
| Departure Headway (Hd) | 7.355 | 7.19 | 8.119 | 6.274 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 494 | 507 | 446 | 580 |
| Service Time | 5.355 | 5.19 | 6.119 | 4.297 |
| HCM Lane V/C Ratio | 0.52 | 0.73 | 0.314 | 1.053 |
| HCM Control Delay | 17.7 | 25.6 | 14.6 | 80.8 |
| HCM Lane LOS | C | D | B | F |
| HCM 95th-tile Q | 2.8 | 5.5 | 1.3 | 17.6 |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 2 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  | ¢ |  |
| Traffic Vol, veh/h | 4 | 213 | 28 | 18 | 225 | 6 | 14 | 2 | 18 | 2 | 5 | 5 |
| Future Vol, veh/h | 4 | 213 | 28 | 18 | 225 | 6 | 14 | 2 | 18 | 2 | 5 | 5 |
| Conflicting Peds, \#hr | 10 | 0 | 0 | 0 | 0 | 10 | 12 | 0 | 5 | 5 | 0 | 12 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - |  | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 64 | 64 | 64 | 78 | 78 | 78 | 57 | 57 | 57 | 42 | 42 | 42 |
| Heavy Vehicles, \% | 1 | , | 1 | 5 | 5 | 5 | 7 | 7 | 7 | 100 | 80 | 0 |
| Mvmt Flow | 6 | 333 | 44 | 23 | 288 | 8 | 25 | 4 | 32 | 5 | 12 | 12 |



| Approach | EB | WB | NB | SB |
| :--- | :--- | :--- | ---: | ---: |
| HCM Control Delay, s | 0.1 | 0.6 | 14.7 | 16.7 |
| HCM LOS |  |  | B | C |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 431 | 1248 | - | -1165 | - | -335 |  |  |
| HCM Lane V/C Ratio | 0.138 | 0.005 | - | - | 0.02 | - | -0.085 |  |
| HCM Control Delay (s) | 14.7 | 7.9 | 0 | - | 8.2 | 0 | -16.7 |  |
| HCM Lane LOS | B | A | A | - | A | A | - | C |
| HCM 95th \%tile Q(veh) | 0.5 | 0 | - | - | 0.1 | - | - | 0.3 |


|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |



| Lane Group | t EBL | $\rightarrow$ | EBR | WBL | « WBT | 4 WBR | ${ }_{\text {NBL }}$ | ${ }_{\text {NBT }}$ | NBR | SBL | ¢ SBT | $\stackrel{\downarrow}{\text { SBR }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | $\uparrow$ | 「 |  | $\uparrow$ | 「 | ${ }^{7}$ | $\hat{\beta}$ |  | ${ }^{7}$ | $\uparrow$ | T |
| Trafic Volume (vph) | 223 | 30 | 198 | 40 | 51 | 62 | 283 | 793 | 30 | 27 | 308 | 120 |
| Future Volume (vph) | 223 | 30 | 198 | 40 | 51 | 62 | 283 | 793 | 30 | 27 | 308 | 120 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 10 | 12 | 10 | 10 | 11 | 11 | 11 | 12 | 10 | 11 | 11 | 12 |
| Storage Length (ft) | 0 |  | 75 | 0 |  | 0 | 60 |  | 0 | 90 |  | 140 |
| Storage Lanes | 0 |  | 1 | 0 |  | 1 | 1 |  | 0 | 1 |  | 1 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  | 0.99 | 0.97 |  | 1.00 | 0.96 | 0.99 | 1.00 |  |  |  | 0.96 |
| Frt |  |  | 0.850 |  |  | 0.850 |  | 0.995 |  |  |  | 0.850 |
| FIt Protected |  | 0.958 |  |  | 0.978 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1785 | 1478 | 0 | 1761 | 1531 | 1711 | 1851 | 0 | 1711 | 1801 | 1583 |
| FIt Permitted |  | 0.684 |  |  | 0.670 |  | 0.562 |  |  | 0.114 |  |  |
| Satd. Flow (perm) | 0 | 1261 | 1428 | 0 | 1203 | 1476 | 1002 | 1851 | 0 | 205 | 1801 | 1527 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  | 171 |  |  | 145 |  | 3 |  |  |  | 128 |
| Link Speed (mph) |  | 30 |  |  | 25 |  |  | 35 |  |  | 35 |  |
| Link Distance (ft) |  | 577 |  |  | 127 |  |  | 874 |  |  | 1332 |  |
| Travel Time (s) |  | 13.1 |  |  | 3.5 |  |  | 17.0 |  |  | 25.9 |  |
| Confl. Peds. (\#/hr) | 6 |  | 5 | 5 |  | 6 | 6 |  | 4 | 4 |  | 6 |
| Confl. Bikes (\#/hr) |  |  | 2 |  |  | 2 |  |  | 3 |  |  | 1 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Adj. Flow (vph) | 237 | 32 | 211 | 43 | 54 | 66 | 301 | 844 | 32 | 29 | 328 | 128 |
| Shared Lane Trafic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 269 | 211 | 0 | 97 | 66 | 301 | 876 | 0 | 29 | 328 | 128 |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | pm+pt | NA |  | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 4 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  | 4 | 4 |  | 4 | 2 |  |  | 6 |  | 6 |
| Detector Phase | 4 | 4 | 4 | 4 | 4 | 4 | 5 | 2 |  | 1 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 | 5.0 | 10.0 |  | 5.0 | 10.0 | 10.0 |
| Minimum Split (s) | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 12.0 | 21.0 |  | 12.0 | 23.0 | 23.0 |
| Total Split (s) | 29.0 | 29.0 | 29.0 | 29.0 | 29.0 | 29.0 | 18.0 | 49.0 |  | 12.0 | 43.0 | 43.0 |
| Total Split (\%) | 32.2\% | 32.2\% | 32.2\% | 32.2\% | 32.2\% | 32.2\% | 20.0\% | 54.4\% |  | 13.3\% | 47.8\% | 47.8\% |
| Maximum Green (s) | 24.0 | 24.0 | 24.0 | 24.0 | 24.0 | 24.0 | 13.0 | 44.0 |  | 7.0 | 38.0 | 38.0 |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) |  | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 |
| Lead/Lag |  |  |  |  |  |  | Lag | Lag |  | Lead | Lead | Lead |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes |  | Yes | Yes | Yes |
| Vehicle Extension (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 |
| Recall Mode | None | None | None | None | None | None | None | C-Max |  | None | C-Max | C-Max |
| Walk Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 |  |  | 7.0 | 7.0 |
| Flash Dont Walk (s) | 13.0 | 13.0 | 13.0 | 13.0 | 13.0 | 13.0 |  | 9.0 |  |  | 11.0 | 11.0 |
| Pedestrian Calls (\#/hr) | 2 | 2 | 2 | 2 | 2 | 2 |  | 0 |  |  | 5 | 5 |
| Act Effct Green (s) |  | 21.6 | 21.6 |  | 21.6 | 21.6 | 53.8 | 53.8 |  | 40.4 | 40.4 | 40.4 |


| Lane Group | EBL | $\rightarrow$ |  | WBL | ↔- | 4 WBR | 4 | 4 NBT | NBR | SBL | ¢ SBT | ¢ SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Actuated g/C Ratio |  | 0.24 | 0.24 |  | 0.24 | 0.24 | 0.60 | 0.60 |  | 0.45 | 0.45 | 0.45 |
| $\mathrm{v} / \mathrm{c}$ Ratio |  | 0.89 | 0.45 |  | 0.34 | 0.14 | 0.43 | 0.79 |  | 0.16 | 0.41 | 0.17 |
| Control Delay |  | 63.7 | 10.3 |  | 30.8 | 0.6 | 15.6 | 23.5 |  | 17.1 | 19.4 | 3.7 |
| Queue Delay |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Delay |  | 63.7 | 10.3 |  | 30.8 | 0.6 | 15.6 | 23.5 |  | 17.1 | 19.4 | 3.7 |
| LOS |  | E | B |  | C | A | B | C |  | B | B | A |
| Approach Delay |  | 40.2 |  |  | 18.6 |  |  | 21.5 |  |  | 15.1 |  |
| Approach LOS |  | D |  |  | B |  |  | C |  |  | B |  |
| Queue Length 50th (ft) |  | 142 | 17 |  | 44 | 0 | 71 | 323 |  | 9 | 128 | 0 |
| Queue Length 95th (ft) |  | \#272 | 75 |  | 88 | 0 | 161 | \#733 |  | 26 | 200 | 32 |
| Internal Link Dist (ft) |  | 497 |  |  | 47 |  |  | 794 |  |  | 1252 |  |
| Turn Bay Length (ft) |  |  | 75 |  |  |  | 60 |  |  | 90 |  | 140 |
| Base Capacity (vph) |  | 336 | 506 |  | 320 | 499 | 701 | 1108 |  | 208 | 808 | 755 |
| Starvation Cap Reductn |  | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 |
| Spillback Cap Reductn |  | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 |
| Storage Cap Reductn |  | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 |
| Reduced v/c Ratio |  | 0.80 | 0.42 |  | 0.30 | 0.13 | 0.43 | 0.79 |  | 0.14 | 0.41 | 0.17 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type: Other
Cycle Length: 90
Actuated Cycle Length: 90
Offset: $0(0 \%)$, Referenced to phase 2:NBTL and 6:SBTL, Start of Green
Natural Cycle: 90
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 0.89
Intersection Signal Delay: $23.8 \quad$ Intersection LOS: C
Intersection Capacity Utilization 83.7\% ICU Level of Service E
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 2: 15th Ave NE \& NE 155th St


| Lane Group | A EBL | $\rightarrow$ | EBR | WBL | - WBT | WBR | 4 NBL | NBT | NBR | SBL | ¢ SBT | $\downarrow$ SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ |  | ${ }^{7}$ | $\uparrow$ |  | \% | $\uparrow$ |  | ${ }^{7}$ | $\hat{F}$ |  |
| Traffic Volume (vph) | 148 | 431 | 42 | 40 | 330 | 53 | 141 | 411 | 91 | 30 | 88 | 66 |
| Future Volume (vph) | 148 | 431 | 42 | 40 | 330 | 53 | 141 | 411 | 91 | 30 | 88 | 66 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 11 | 11 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Storage Length (ft) | 110 |  | 0 | 100 |  | 0 | 105 |  | 0 | 160 |  | 0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 0.99 |  |
| Frt |  | 0.987 |  |  | 0.979 |  |  | 0.973 |  |  | 0.936 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1770 | 1773 | 0 | 1770 | 1817 | 0 | 1770 | 1805 | 0 | 1687 | 1646 | 0 |
| Flt Permitted | 0.411 |  |  | 0.299 |  |  | 0.650 |  |  | 0.277 |  |  |
| Satd. Flow (perm) | 764 | 1773 | 0 | 556 | 1817 | 0 | 1209 | 1805 | 0 | 491 | 1646 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 10 |  |  | 17 |  |  | 26 |  |  | 73 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 572 |  |  | 796 |  |  | 673 |  |  | 531 |  |
| Travel Time (s) |  | 13.0 |  |  | 18.1 |  |  | 15.3 |  |  | 12.1 |  |
| Confl. Peds. (\#/hr) | 3 |  | 3 | 3 |  | 3 | 1 |  | 2 | 2 |  | 1 |
| Confl. Bikes (\#/hr) |  |  | 2 |  |  | 2 |  |  |  |  |  | 1 |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 7\% | 7\% | 7\% |
| Adj. Flow (vph) | 163 | 474 | 46 | 44 | 363 | 58 | 155 | 452 | 100 | 33 | 97 | 73 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 163 | 520 | 0 | 44 | 421 | 0 | 155 | 552 | 0 | 33 | 170 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 2 |  |  | 2 |  |  | 4 |  |  | 4 |  |
| Permitted Phases | 2 |  |  | 2 |  |  | 4 |  |  | 4 |  |  |
| Detector Phase | 2 | 2 |  | 2 | 2 |  | 4 | 4 |  | 4 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Minimum Split (s) | 24.0 | 24.0 |  | 24.0 | 24.0 |  | 24.0 | 24.0 |  | 24.0 | 24.0 |  |
| Total Split (s) | 26.0 | 26.0 |  | 26.0 | 26.0 |  | 29.0 | 29.0 |  | 29.0 | 29.0 |  |
| Total Split (\%) | 47.3\% | 47.3\% |  | 47.3\% | 47.3\% |  | 52.7\% | 52.7\% |  | 52.7\% | 52.7\% |  |
| Maximum Green (s) | 21.0 | 21.0 |  | 21.0 | 21.0 |  | 24.0 | 24.0 |  | 24.0 | 24.0 |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Recall Mode | None | None |  | None | None |  | None | None |  | None | None |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 12.0 | 12.0 |  | 12.0 | 12.0 |  | 12.0 | 12.0 |  | 12.0 | 12.0 |  |
| Pedestrian Calls (\#/hr) | 5 | 5 |  | 5 | 5 |  | 7 | 7 |  | 7 | 7 |  |
| Act Effct Green (s) | 17.5 | 17.5 |  | 17.5 | 17.5 |  | 18.1 | 18.1 |  | 18.1 | 18.1 |  |


| Lane Group | - EBL | $\rightarrow$ |  | WBL | - WBT |  | NBL | 4 NBT | NBR | SBL | $\frac{1}{*}$ SBT | ¢ SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Actuated g/C Ratio | 0.38 | 0.38 |  | 0.38 | 0.38 |  | 0.39 | 0.39 |  | 0.39 | 0.39 |  |
| $\mathrm{v} / \mathrm{C}$ Ratio | 0.57 | 0.77 |  | 0.21 | 0.60 |  | 0.33 | 0.76 |  | 0.17 | 0.25 |  |
| Control Delay | 22.1 | 23.1 |  | 14.2 | 16.3 |  | 12.5 | 19.9 |  | 12.2 | 7.1 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 22.1 | 23.1 |  | 14.2 | 16.3 |  | 12.5 | 19.9 |  | 12.2 | 7.1 |  |
| LOS | C | C |  | B | B |  | B | B |  | B | A |  |
| Approach Delay |  | 22.8 |  |  | 16.1 |  |  | 18.3 |  |  | 7.9 |  |
| Approach LOS |  | C |  |  | B |  |  | B |  |  | A |  |
| Queue Length 50th (ft) | 35 | 122 |  | 8 | 89 |  | 31 | 130 |  | 6 | 18 |  |
| Queue Length 95th (ft) | \#101 | \#282 |  | 30 | 179 |  | 66 | 228 |  | 21 | 48 |  |
| Internal Link Dist (ft) |  | 492 |  |  | 716 |  |  | 593 |  |  | 451 |  |
| Turn Bay Length (ft) | 110 |  |  | 100 |  |  | 105 |  |  | 160 |  |  |
| Base Capacity (vph) | 369 | 863 |  | 269 | 888 |  | 669 | 1010 |  | 271 | 943 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.44 | 0.60 |  | 0.16 | 0.47 |  | 0.23 | 0.55 |  | 0.12 | 0.18 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type: Other

Cycle Length: 55
Actuated Cycle Length: 46.2
Natural Cycle: 50
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.77
Intersection Signal Delay: 18.3
Intersection LOS: B
Intersection Capacity Utilization 77.5\% ICU Level of Service D
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 3: 5th Ave NE \& NE 155th St


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 17.7 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS | C |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | ¢ |  |  | $\uparrow$ |  |  | $\dagger$ |  |
| Traffic Vol, veh/h | 153 | 48 | 39 | 5 | 13 | 5 | 52 | 412 | 4 | 5 | 109 | 54 |
| Future Vol, veh/h | 153 | 48 | 39 | 5 | 13 | 5 | 52 | 412 | 4 | 5 | 109 | 54 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.75 | 0.75 | 0.75 | 0.87 | 0.87 | 0.87 | 0.75 | 0.75 | 0.75 |
| Heavy Vehicles, \% | 1 | 1 | 1 | 5 | 5 | 5 | 0 | 0 | 0 | 1 | 1 | 1 |
| Mumt Flow | 158 | 49 | 40 | 7 | 17 | 7 | 60 | 474 | 5 | 7 | 145 | 72 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 13.1 |  |  | 9.9 |  |  | 23 |  |  | 11.1 |  |  |
| HCM LOS | B |  |  | A |  |  | C |  |  | B |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $11 \%$ | $64 \%$ | $22 \%$ | $3 \%$ |
| Vol Thru, \% | $88 \%$ | $20 \%$ | $57 \%$ | $65 \%$ |
| Vol Right, \% | $1 \%$ | $16 \%$ | $22 \%$ | $32 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 468 | 240 | 23 | 168 |
| LT Vol | 52 | 153 | 5 | 5 |
| Through Vol | 412 | 48 | 13 | 109 |
| RT Vol | 4 | 39 | 5 | 54 |
| Lane Flow Rate | 538 | 247 | 31 | 224 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.766 | 0.41 | 0.055 | 0.335 |
| Departure Headway (Hd) | 5.127 | 5.961 | 6.44 | 5.381 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 705 | 601 | 553 | 665 |
| Service Time | 3.167 | 4.015 | 4.518 | 3.433 |
| HCM Lane V/C Ratio | 0.763 | 0.411 | 0.056 | 0.337 |
| HCM Control Delay | 23 | 13.1 | 9.9 | 11.1 |
| HCM Lane LOS | C | B | A | B |
| HCM 95th-tile Q | 7.2 | 2 | 0.2 | 1.5 |



| Major/Minor | Major1 | Major2 |  |  |  | Minor1 |  |  | Minor2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 146 | 0 | 0 | 261 | 0 | 0 | 432 | 429 | 255 | 475 | 434 | 143 |
| Stage 1 | - | - | - | - | - | - | 259 | 259 | - | 165 | 165 | - |
| Stage 2 | - | - | - | - | - | - | 173 | 170 | - | 310 | 269 | $\stackrel{-}{-}$ |
| Critical Hdwy | 4.12 | - | - | 4.13 | - | - | 7.12 | 6.52 | 6.22 | 7.1 | 6.5 | 6.2 |
| Critical Hdwy Stg 1 |  | - | - | - | - | - | 6.12 | 5.52 | - | 6.1 | 5.5 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.12 | 5.52 | - | 6.1 | 5.5 | - |
| Follow-up Hdwy | 2.218 | - | - | 2.227 | - | - | 3.518 | 4.018 | 3.318 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 1436 | - | - | 1298 | - | - | 534 | 518 | 784 | 503 | 518 | 910 |
| Stage 1 | - | - | - | - | - | - | 746 | 694 | - | 842 | 766 | - |
| Stage 2 | - | - | - | - | - | - | 829 | 758 | - | 705 | 690 | - |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | 1428 | - | - | 1298 | - | - | 512 | 508 | 781 | 434 | 508 | 903 |
| Mov Cap-2 Maneuver |  | - | - | - | - | - | 512 | 508 | - | 434 | 508 | - |
| Stage 1 | - | - | - | - | - | - | 744 | 692 | - | 834 | 754 | - |
| Stage 2 | - | - | - | - | - | - | 795 | 746 | - | 616 | 688 | - |


| Approach | EB | WB | NB | SB |
| :--- | :--- | :--- | ---: | ---: |
| HCM Control Delay, s | 0.1 | 0.6 | 12 | 11.5 |
| HCM LOS |  |  | B | B |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 653 | 1428 | - | -1298 | - | -589 |  |
| HCM Lane V/C Ratio | 0.218 | 0.003 | - | -0.009 | - | -0.062 |  |
| HCM Control Delay (s) | 12 | 7.5 | 0 | - | 7.8 | 0 | -11.5 |
| HCM Lane LOS | $B$ | A | A | - | A | A | - |
| HCM 95th \%tile Q(veh) | 0.8 | 0 | - | - | 0 | - | - |
| B |  | 0.2 |  |  |  |  |  |


| Lane Group | FBL | $\rightarrow$ | EBR | WBL | - |  | 4 | ¢ ${ }_{\text {NBT }}$ | NBR |  | $\stackrel{1}{\dagger}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | ¢ |  |  | $\uparrow$ |  | \% | 个 ${ }^{\text {a }}$ |  | \% | 个 ${ }^{\text {a }}$ |  |
| Traffic Volume (vph) | 1 | , | 3 | 68 | 4 | 155 |  | 366 | 127 | 166 | 923 | 2 |
| Future Volume (vph) | 1 | 4 | 3 | 68 | 4 | 155 | 3 | 366 | 127 | 166 | 923 | 2 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 11 | 11 | 11 | 12 | 11 | 11 | 12 | 11 | 11 |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 45 |  | 0 | 80 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 |
| Ped Bike Factor |  | 0.99 |  |  | 0.98 |  |  | 0.99 |  | 0.99 | 1.00 |  |
| Frt |  | 0.949 |  |  | 0.908 |  |  | 0.961 |  |  |  |  |
| Flt Protected |  | 0.994 |  |  | 0.985 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1780 | 0 | 0 | 1526 | 0 | 1752 | 3223 | 0 | 1752 | 3387 | 0 |
| FIt Permitted |  | 0.994 |  |  | 0.985 |  | 0.209 |  |  | 0.463 |  |  |
| Satd. Flow (perm) | 0 | 1778 | 0 | 0 | 1522 | 0 | 386 | 3223 | 0 | 846 | 3387 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 3 |  |  | 89 |  |  | 50 |  |  |  |  |
| Link Speed (mph) |  | 10 |  |  | 30 |  |  | 35 |  |  | 35 |  |
| Link Distance (ft) |  | 100 |  |  | 1323 |  |  | 672 |  |  | 440 |  |
| Travel Time (s) |  | 6.8 |  |  | 30.1 |  |  | 13.1 |  |  | 8.6 |  |
| Confl. Peds. (\#/hr) | 6 |  | 4 | 4 |  | 6 | 24 |  | 7 | 7 |  | 24 |
| Confl. Bikes (\#/hr) |  |  |  |  |  | 1 |  |  |  |  |  | 1 |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Heavy Vehicles (\%) | 0\% | 0\% | 0\% | 6\% | 6\% | 6\% | 3\% | 3\% | 3\% | 3\% | 3\% | 3\% |
| Adj. Flow (vph) | 1 | 4 | 3 | 71 | 4 | 161 | 3 | 381 | 132 | 173 | 961 | 2 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 8 | 0 | 0 | 236 | 0 | 3 | 513 | 0 | 173 | 963 | 0 |
| Turn Type | Split | NA |  | Split | NA |  | pm+pt | NA |  | pm+pt | NA |  |
| Protected Phases | 4 | 4 |  | 3 | 3 |  | 1 | 6 |  | 5 | 2 |  |
| Permitted Phases |  |  |  |  |  |  | 6 |  |  | 2 |  |  |
| Detector Phase | 4 | 4 |  | 3 | 3 |  | 1 | 6 |  | 5 | 2 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 10.0 | 10.0 |  | 5.0 | 15.0 |  | 5.0 | 15.0 |  |
| Minimum Split (s) | 24.0 | 24.0 |  | 25.0 | 25.0 |  | 12.0 | 25.0 |  | 12.0 | 20.0 |  |
| Total Split (s) | 24.0 | 24.0 |  | 28.0 | 28.0 |  | 12.0 | 46.0 |  | 12.0 | 46.0 |  |
| Total Split (\%) | 21.8\% | 21.8\% |  | 25.5\% | 25.5\% |  | 10.9\% | 41.8\% |  | 10.9\% | 41.8\% |  |
| Maximum Green (s) | 19.0 | 19.0 |  | 23.0 | 23.0 |  | 7.0 | 41.0 |  | 7.0 | 41.0 |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) |  | 0.0 |  |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) |  | 5.0 |  |  | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Lead/Lag | Lag | Lag |  | Lead | Lead |  | Lead | Lead |  | Lag | Lag |  |
| Lead-Lag Optimize? | Yes | Yes |  | Yes | Yes |  | Yes | Yes |  | Yes | Yes |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None |  | None | C-Max |  | None | C-Max |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  |  | 7.0 |  |  | 7.0 |  |
| Flash Dont Walk (s) | 12.0 | 12.0 |  | 13.0 | 13.0 |  |  | 13.0 |  |  | 6.0 |  |
| Pedestrian Calls (\#hr) | 8 | 8 |  | 4 | 4 |  |  | 7 |  |  | 14 |  |
| Act Effct Green (s) |  | 8.4 |  |  | 16.5 |  | 64.5 | 64.5 |  | 74.3 | 74.3 |  |


| Lane Group | EBL | $\rightarrow$ |  | WBL | $*$ WBT |  | 4 | 4 <br> NBT | NBR | SBL | t SBT | ¢ SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Actuated g/C Ratio |  | 0.08 |  |  | 0.15 |  | 0.59 | 0.59 |  | 0.68 | 0.68 |  |
| v/c Ratio |  | 0.06 |  |  | 0.78 |  | 0.01 | 0.27 |  | 0.28 | 0.42 |  |
| Control Delay |  | 36.2 |  |  | 44.6 |  | 17.7 | 13.1 |  | 14.6 | 12.9 |  |
| Queue Delay |  | 0.0 |  |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay |  | 36.2 |  |  | 44.6 |  | 17.7 | 13.1 |  | 14.6 | 12.9 |  |
| LOS |  | D |  |  | D |  | B | B |  | B | B |  |
| Approach Delay |  | 36.3 |  |  | 44.6 |  |  | 13.2 |  |  | 13.2 |  |
| Approach LOS |  | D |  |  | D |  |  | B |  |  | B |  |
| Queue Length 50th (ft) |  | 3 |  |  | 101 |  | 1 | 64 |  | 27 | 101 |  |
| Queue Length 95th (ft) |  | 17 |  |  | 180 |  | 8 | 172 |  | 136 | 384 |  |
| Internal Link Dist (tt) |  | 20 |  |  | 1243 |  |  | 592 |  |  | 360 |  |
| Turn Bay Length (ft) |  |  |  |  |  |  | 45 |  |  | 80 |  |  |
| Base Capacity (vph) |  | 309 |  |  | 389 |  | 313 | 1909 |  | 628 | 2286 |  |
| Starvation Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spill back Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio |  | 0.03 |  |  | 0.61 |  | 0.01 | 0.27 |  | 0.28 | 0.42 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type: Other
Cycle Length: 110
Actuated Cycle Length: 110
Offset: 14 (13\%), Referenced to phase 2:SBTL and 6:NBTL, Start of Green
Natural Cycle: 90
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 0.78

Intersection Signal Delay: 17.2
Intersection Capacity Utilization 62.9\%
Analysis Period (min) 15

Intersection LOS: B
ICU Level of Service B

Splits and Phases: 1: 15th Ave NE \& NE 150th St


| Lane Group | EBL | $\rightarrow$ | EBR | WBL | $\leftarrow$ WBT |  | 4 | $\uparrow$ NBT | NBR | SBL | $\frac{1}{*}$ SBT | $\stackrel{\downarrow}{\text { SBR }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | $\uparrow$ | \% |  | $\uparrow$ | \% | ${ }^{7}$ | $\hat{\beta}$ |  | ${ }^{7}$ | $\uparrow$ | F |
| Traffic Volume (vph) | 63 | 35 | 281 | 5 | 7 | 10 | 220 | 273 | 36 | 107 | 923 | 344 |
| Future Volume (vph) | 63 | 35 | 281 | 5 | 7 | 10 | 220 | 273 | 36 | 107 | 923 | 344 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 10 | 12 | 10 | 10 | 11 | 11 | 11 | 12 | 10 | 11 | 11 | 12 |
| Storage Length (ft) | 0 |  | 75 | 0 |  | 0 | 60 |  | 0 | 90 |  | 140 |
| Storage Lanes | 0 |  | 1 | 0 |  | 1 | 1 |  | 0 | 1 |  | 1 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  | 1.00 | 0.97 |  | 1.00 | 0.97 | 1.00 | 1.00 |  | 1.00 |  | 0.97 |
| Frt |  |  | 0.850 |  |  | 0.850 |  | 0.983 |  |  |  | 0.850 |
| Flt Protected |  | 0.969 |  |  | 0.980 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1805 | 1478 | 0 | 1271 | 994 | 1662 | 1774 | 0 | 1711 | 1801 | 1583 |
| Flt Permitted |  | 0.798 |  |  | 0.905 |  | 0.095 |  |  | 0.453 |  |  |
| Satd. Flow (perm) | 0 | 1482 | 1438 | 0 | 1172 | 968 | 166 | 1774 | 0 | 815 | 1801 | 1530 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  | 280 |  |  | 145 |  | 11 |  |  |  | 197 |
| Link Speed (mph) |  | 30 |  |  | 25 |  |  | 35 |  |  | 35 |  |
| Link Distance (ft) |  | 577 |  |  | 127 |  |  | 874 |  |  | 1332 |  |
| Travel Time (s) |  | 13.1 |  |  | 3.5 |  |  | 17.0 |  |  | 25.9 |  |
| Confl. Peds. (\#/hr) | 2 |  | 1 | 1 |  | 2 | 5 |  | 1 | 1 |  | 5 |
| Confl. Bikes (\#/hr) |  |  | 3 |  |  | 1 |  |  | 2 |  |  | 2 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 100\% | 0\% | 57\% | 5\% | 5\% | 5\% | 2\% | 2\% | 2\% |
| Adj. Flow (vph) | 67 | 37 | 299 | 5 | 7 | 11 | 234 | 290 | 38 | 114 | 982 | 366 |
| Shared Lane Trafic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 104 | 299 | 0 | 12 | 11 | 234 | 328 | 0 | 114 | 982 | 366 |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | pm+pt | NA |  | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 4 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  | 4 | 4 |  | 4 | 2 |  |  | 6 |  | 6 |
| Detector Phase | 4 | 4 | 4 | 4 | 4 | 4 | 5 | 2 |  | 1 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 | 5.0 | 10.0 |  | 5.0 | 10.0 | 10.0 |
| Minimum Split (s) | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 12.0 | 21.0 |  | 12.0 | 23.0 | 23.0 |
| Total Split (s) | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 15.0 | 53.0 |  | 12.0 | 50.0 | 50.0 |
| Total Split (\%) | 27.8\% | 27.8\% | 27.8\% | 27.8\% | 27.8\% | 27.8\% | 16.7\% | 58.9\% |  | 13.3\% | 55.6\% | 55.6\% |
| Maximum Green (s) | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 | 10.0 | 48.0 |  | 7.0 | 45.0 | 45.0 |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) |  | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 |
| Lead/Lag |  |  |  |  |  |  | Lag | Lag |  | Lead | Lead | Lead |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes |  | Yes | Yes | Yes |
| Vehicle Extension (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 |
| Recall Mode | None | None | None | None | None | None | None | C-Max |  | None | C-Max | C-Max |
| Walk Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 |  |  | 7.0 | 7.0 |
| Flash Dont Walk (s) | 13.0 | 13.0 | 13.0 | 13.0 | 13.0 | 13.0 |  | 9.0 |  |  | 11.0 | 11.0 |
| Pedestrian Calls (\#/hr) | 2 | 2 | 2 | 2 | 2 | 2 |  | 0 |  |  | 5 | 5 |



Area Type: Other
Cycle Length: 90
Actuated Cycle Length: 90
Offset: $0(0 \%)$, Referenced to phase 2:NBTL and 6:SBTL, Start of Green
Natural Cycle: 90
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 1.00
Intersection Signal Delay: $32.9 \quad$ Intersection LOS: C
Intersection Capacity Utilization 91.4\% ICU Level of Service F
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 2: 15th Ave NE \& NE 155th St


| Lane Group | t EBL | $\rightarrow \underset{\text { EBT }}{\rightarrow}$ | EBR | WBL | $\leftarrow$ WBT | WBR | ${ }_{\text {NBL }}$ | ¢ NBT | NBR | SBL | $\downarrow$ SBT | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | $\dagger$ |  | ${ }^{7}$ | $\dagger$ |  | ${ }^{7}$ | $\hat{F}$ |  | ${ }^{7}$ | $\dagger$ |  |
| Traffic Volume (vph) | 62 | 264 | 79 | 155 | 441 | 24 | 120 | 80 | 41 | 68 | 420 | 176 |
| Future Volume (vph) | 62 | 264 | 79 | 155 | 441 | 24 | 120 | 80 | 41 | 68 | 420 | 176 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 11 | 11 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Storage Length (ft) | 110 |  | 0 | 100 |  | 0 | 105 |  | 0 | 160 |  | 0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | 1.00 | 0.99 |  | 1.00 | 1.00 |  | 1.00 |  |  |  | 0.99 |  |
| Frt |  | 0.966 |  |  | 0.992 |  |  | 0.949 |  |  | 0.956 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1703 | 1664 | 0 | 1736 | 1810 | 0 | 1703 | 1701 | 0 | 1687 | 1686 | 0 |
| Flt Permitted | 0.308 |  |  | 0.464 |  |  | 0.225 |  |  | 0.676 |  |  |
| Satd. Flow (perm) | 550 | 1664 | 0 | 845 | 1810 | 0 | 403 | 1701 | 0 | 1200 | 1686 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 32 |  |  | 6 |  |  | 43 |  |  | 49 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 572 |  |  | 796 |  |  | 673 |  |  | 531 |  |
| Travel Time (s) |  | 13.0 |  |  | 18.1 |  |  | 15.3 |  |  | 12.1 |  |
| Confl. Peds. (\#/hr) | 5 |  | 4 | 4 |  | 5 | 2 |  |  |  |  | 2 |
| Confl. Bikes (\#hr) |  |  | 1 |  |  |  |  |  |  |  |  | 1 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles (\%) | 6\% | 6\% | 6\% | 4\% | 4\% | 4\% | 6\% | 6\% | 6\% | 7\% | 7\% | 7\% |
| Adj. Flow (vph) | 65 | 278 | 83 | 163 | 464 | 25 | 126 | 84 | 43 | 72 | 442 | 185 |
| Shared Lane Trafic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 65 | 361 | 0 | 163 | 489 | 0 | 126 | 127 | 0 | 72 | 627 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 2 |  |  | 2 |  |  | 4 |  |  | 4 |  |
| Permitted Phases | 2 |  |  | 2 |  |  | 4 |  |  | 4 |  |  |
| Detector Phase | 2 | 2 |  |  | 2 |  | 4 | 4 |  | 4 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Minimum Split (s) | 24.0 | 24.0 |  | 24.0 | 24.0 |  | 24.0 | 24.0 |  | 24.0 | 24.0 |  |
| Total Split (s) | 26.0 | 26.0 |  | 26.0 | 26.0 |  | 29.0 | 29.0 |  | 29.0 | 29.0 |  |
| Total Split (\%) | 47.3\% | 47.3\% |  | 47.3\% | 47.3\% |  | 52.7\% | 52.7\% |  | 52.7\% | 52.7\% |  |
| Maximum Green (s) | 21.0 | 21.0 |  | 21.0 | 21.0 |  | 24.0 | 24.0 |  | 24.0 | 24.0 |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Recall Mode | None | None |  | None | None |  | None | None |  | None | None |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 12.0 | 12.0 |  | 12.0 | 12.0 |  | 12.0 | 12.0 |  | 12.0 | 12.0 |  |
| Pedestrian Calls (\#/hr) | 5 | 5 |  | 5 | 5 |  | 7 | 7 |  | 7 | 7 |  |
| Act Effct Green (s) | 17.2 | 17.2 |  | 17.2 | 17.2 |  | 20.2 | 20.2 |  | 20.2 | 20.2 |  |


| Lane Group | E EBL | $\rightarrow$ |  | WBL | - WBT |  | 4 | 4 NBT | NBR | SBL | $\frac{1}{*}$ SBT | $\stackrel{ }{\text { ¢ }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Actuated g/C Ratio | 0.36 | 0.36 |  | 0.36 | 0.36 |  | 0.42 | 0.42 |  | 0.42 | 0.42 |  |
| $\mathrm{v} / \mathrm{c}$ Ratio | 0.33 | 0.58 |  | 0.54 | 0.75 |  | 0.75 | 0.17 |  | 0.14 | 0.85 |  |
| Control Delay | 17.5 | 16.3 |  | 20.8 | 22.4 |  | 44.6 | 7.4 |  | 10.2 | 25.9 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 17.5 | 16.3 |  | 20.8 | 22.4 |  | 44.6 | 7.4 |  | 10.2 | 25.9 |  |
| LOS | B | B |  | C | C |  | D | A |  | B | C |  |
| Approach Delay |  | 16.4 |  |  | 22.0 |  |  | 25.9 |  |  | 24.2 |  |
| Approach LOS |  | B |  |  | C |  |  | C |  |  | C |  |
| Queue Length 50th (ft) | 14 | 80 |  | 39 | 129 |  | 32 | 15 |  | 13 | 157 |  |
| Queue Length 95th (ft) | 42 | 150 |  | 91 | \#229 |  | \#114 | 41 |  | 34 | \#334 |  |
| Internal Link Dist (ft) |  | 492 |  |  | 716 |  |  | 593 |  |  | 451 |  |
| Turn Bay Length (ft) | 110 |  |  | 100 |  |  | 105 |  |  | 160 |  |  |
| Base Capacity (vph) | 254 | 786 |  | 390 | 839 |  | 212 | 918 |  | 633 | 913 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |  | 0 |  |
| Reduced v/c Ratio | 0.26 | 0.46 |  | 0.42 | 0.58 |  | 0.59 | 0.14 |  | 0.11 | 0.69 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type: Other

Cycle Length: 55
Actuated Cycle Length: 48
Natural Cycle: 55
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.85

Intersection Signal Delay: 22.1
Intersection LOS: C
ICU Level of Service E

Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 3: 5th Ave NE \& NE 155th St


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh Intersection LOS | $\begin{array}{r} 126.5 \\ F \end{array}$ |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | $\dagger$ |  |  | ${ }_{\$}$ |  |  | \$ |  |
| Traffic Vol, veh/h | 230 | 33 | 110 | 31 | 44 | 13 | 61 | 166 | 1 | 3 | 311 | 156 |
| Future Vol, veh/h | 230 | 33 | 110 | 31 | 44 | 13 | 61 | 166 | 1 | 3 | 311 | 156 |
| Peak Hour Factor | 0.64 | 0.64 | 0.64 | 0.63 | 0.63 | 0.63 | 0.63 | 0.63 | 0.63 | 0.73 | 0.73 | 0.73 |
| Heavy Vehicles, \% | 1 | 1 | 1 | 5 | 5 | 5 | 0 | 0 | 0 | 1 | 1 | 1 |
| Mvmt Flow | 359 | 52 | 172 | 49 | 70 | 21 | 97 | 263 | 2 | 4 | 426 | 214 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 143.9 |  |  | 19.5 |  |  | 39.8 |  |  | 182.8 |  |  |
| HCM LOS | F |  |  | C |  |  | E |  |  | F |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $27 \%$ | $62 \%$ | $35 \%$ | $1 \%$ |
| Vol Thru, \% | $73 \%$ | $9 \%$ | $50 \%$ | $66 \%$ |
| Vol Right, \% | $0 \%$ | $29 \%$ | $15 \%$ | $33 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 228 | 373 | 88 | 470 |
| LT Vol | 61 | 230 | 31 | 3 |
| Through Vol | 166 | 33 | 44 | 311 |
| RT Vol | 1 | 110 | 13 | 156 |
| Lane Flow Rate | 362 | 583 | 140 | 644 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.794 | 1.219 | 0.351 | 1.32 |
| Departure Headway (Hd) | 9.28 | 8.25 | 10.751 | 8.025 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 394 | 443 | 337 | 457 |
| Service Time | 7.28 | 6.25 | 8.751 | 6.025 |
| HCM Lane V/C Ratio | 0.919 | 1.316 | 0.415 | 1.409 |
| HCM Control Delay | 39.8 | 143.9 | 19.5 | 182.8 |
| HCM Lane LOS | E | F | C | F |
| HCM 95th-tile Q | 6.9 | 21.3 | 1.5 | 26.4 |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 2.6 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \$ |  |  | $\dagger$ |  |  | * |  |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 5 | 267 | 35 | 23 | 282 | 8 | 18 | 3 | 23 | 3 | 6 | 6 |
| Future Vol, veh/h | 5 | 267 | 35 | 23 | 282 | 8 | 18 | 3 | 23 | 3 | 6 | 6 |
| Conflicting Peds, \#hr | 10 | 0 | 0 | 0 | 0 | 10 | 12 | 0 | 5 | 5 | 0 | 12 |
| Sign Control F | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - |  |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 64 | 64 | 64 | 78 | 78 | 78 | 57 | 57 | 57 | 42 | 42 | 42 |
| Heavy Vehicles, \% | 1 | 1 | 1 | 5 | 5 | 5 | 7 | 7 | 7 | 100 | 80 | 0 |
| Mvmt Flow | 8 | 417 | 55 | 29 | 362 | 10 | 32 | 5 | 40 | 7 | 14 | 14 |



| Approach | EB | WB | NB | SB |
| :--- | :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0.1 | 0.6 | 19 | 22 |
| HCM LOS |  |  | $C$ | $C$ |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 333 | 1171 | - | -1074 | - | -247 |  |  |
| HCM Lane V/C Ratio | 0.232 | 0.007 | - | -0.027 | - | -0.145 |  |  |
| HCM Control Delay (s) | 19 | 8.1 | 0 | - | 8.4 | 0 | - | 22 |
| HCM Lane LOS | C | A | A | - | A | A | - | C |
| HCM 95th \%tile Q(veh) | 0.9 | 0 | - | - | 0.1 | - | - | 0.5 |


| Lane Group | - | $\rightarrow$ | EBR | WBL | - | ( 4 | 4 | ¢ NBT | NBR | SBL | ¢ SBT | $\stackrel{\downarrow}{\text { SBR }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | ¢ |  |  | ¢ |  | 7 | 性 |  | 7 | 性 |  |
| Traffic Volume (vph) | 5 | , | 11 | 52 | 1 | 148 |  | 1217 | 114 | 95 | 521 | 8 |
| Future Volume (vph) | 5 | 0 | 11 | 52 | 1 | 148 | 6 | 1217 | 114 | 95 | 521 | 8 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 11 | 11 | 11 | 12 | 11 | 11 | 12 | 11 | 11 |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 45 |  | 0 | 80 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 |
| Ped Bike Factor |  | 0.99 |  |  | 0.98 |  | 0.99 | 1.00 |  |  | 1.00 |  |
| Frt |  | 0.907 |  |  | 0.901 |  |  | 0.987 |  |  | 0.998 |  |
| Flt Protected |  | 0.985 |  |  | 0.987 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1679 | 0 | 0 | 1576 | 0 | 1787 | 3401 | 0 | 1770 | 3411 | 0 |
| Flt Permitted |  | 0.985 |  |  | 0.987 |  | 0.391 |  |  | 0.125 |  |  |
| Satd. Flow (perm) | 0 | 1676 | 0 | 0 | 1575 | 0 | 727 | 3401 | 0 | 233 | 3411 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 169 |  |  | 113 |  |  | 10 |  |  | 2 |  |
| Link Speed (mph) |  | 10 |  |  | 30 |  |  | 35 |  |  | 35 |  |
| Link Distance (ft) |  | 100 |  |  | 1323 |  |  | 672 |  |  | 440 |  |
| Travel Time (s) |  | 6.8 |  |  | 30.1 |  |  | 13.1 |  |  | 8.6 |  |
| Confl. Peds. (\#/hr) | 5 |  | 2 | 2 |  | 5 | 12 |  | 4 | 4 |  | 12 |
| Confl. Bikes (\#hr) |  |  |  |  |  | 1 |  |  |  |  |  | 1 |
| Peak Hour Factor | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Heavy Vehicles (\%) | 0\% | 0\% | 0\% | 2\% | 2\% | 2\% | 1\% | 1\% | 1\% | 2\% | 2\% | 2\% |
| Adj. Flow (vph) | 5 | 0 | 11 | 53 | 1 | 151 | 6 | 1242 | 116 | 97 | 532 | 8 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 16 | 0 | 0 | 205 | 0 | 6 | 1358 | 0 | 97 | 540 | 0 |
| Turn Type | Split | NA |  | Split | NA |  | pm+pt | NA |  | pm+pt | NA |  |
| Protected Phases | 4 | 4 |  | 3 | 3 |  | 1 | 6 |  | 5 | 2 |  |
| Permitted Phases |  |  |  |  |  |  | 6 |  |  | 2 |  |  |
| Detector Phase | 4 | 4 |  | 3 | 3 |  | 1 | 6 |  | 5 | 2 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 10.0 | 10.0 |  | 5.0 | 15.0 |  | 5.0 | 15.0 |  |
| Minimum Split (s) | 24.0 | 24.0 |  | 25.0 | 25.0 |  | 12.0 | 25.0 |  | 12.0 | 20.0 |  |
| Total Split (s) | 24.0 | 24.0 |  | 26.0 | 26.0 |  | 12.0 | 48.0 |  | 12.0 | 48.0 |  |
| Total Split (\%) | 21.8\% | 21.8\% |  | 23.6\% | 23.6\% |  | 10.9\% | 43.6\% |  | 10.9\% | 43.6\% |  |
| Maximum Green (s) | 19.0 | 19.0 |  | 21.0 | 21.0 |  | 7.0 | 43.0 |  | 7.0 | 43.0 |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) |  | 0.0 |  |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) |  | 5.0 |  |  | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Lead/Lag | Lag | Lag |  | Lead | Lead |  | Lead | Lead |  | Lag | Lag |  |
| Lead-Lag Optimize? | Yes | Yes |  | Yes | Yes |  | Yes | Yes |  | Yes | Yes |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None |  | None | C-Max |  | None | C-Max |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  |  | 7.0 |  |  | 7.0 |  |
| Flash Dont Walk (s) | 12.0 | 12.0 |  | 13.0 | 13.0 |  |  | 13.0 |  |  | 6.0 |  |
| Pedestrian Calls (\#/hr) | 8 | 8 |  | 4 | 4 |  |  | 7 |  |  | 14 |  |
| Act Effct Green (s) |  | 8.2 |  |  | 13.5 |  | 65.5 | 65.5 |  | 75.2 | 75.2 |  |


| Lane Group | EBL | $\rightarrow$ |  | WBL | $\leftarrow$ WBT |  | 4 | 4 NBT | NBR | SBL | $\downarrow$ SBT | $\stackrel{ }{\downarrow}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Actuated g/C Ratio |  | 0.07 |  |  | 0.12 |  | 0.60 | 0.60 |  | 0.68 | 0.68 |  |
| v/c Ratio |  | 0.06 |  |  | 0.70 |  | 0.01 | 0.67 |  | 0.38 | 0.23 |  |
| Control Delay |  | 0.4 |  |  | 33.6 |  | 15.7 | 20.0 |  | 23.8 | 10.0 |  |
| Queue Delay |  | 0.0 |  |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay |  | 0.4 |  |  | 33.6 |  | 15.7 | 20.0 |  | 23.8 | 10.0 |  |
| LOS |  | A |  |  | C |  | B | C |  | C | B |  |
| Approach Delay |  | 0.4 |  |  | 33.6 |  |  | 20.0 |  |  | 12.1 |  |
| Approach LOS |  | A |  |  | C |  |  | B |  |  | B |  |
| Queue Length 50th (ft) |  | 0 |  |  | 62 |  | 2 | 317 |  | 19 | 62 |  |
| Queue Length 95th (ft) |  | 0 |  |  | 134 |  | 11 | \#660 |  | 78 | 184 |  |
| Internal Link Dist (ft) |  | 20 |  |  | 1243 |  |  | 592 |  |  | 360 |  |
| Turn Bay Length (t) |  |  |  |  |  |  | 45 |  |  | 80 |  |  |
| Base Capacity (vph) |  | 429 |  |  | 392 |  | 500 | 2028 |  | 257 | 2333 |  |
| Starvation Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio |  | 0.04 |  |  | 0.52 |  | 0.01 | 0.67 |  | 0.38 | 0.23 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type: Other
Cycle Length: 110
Actuated Cycle Length: 110
Offset: 14 (13\%), Referenced to phase 2:SBTL and 6:NBTL, Start of Green
Natural Cycle: 100
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 0.70
Intersection Signal Delay: 18.9
Intersection Capacity Utilization 70.6\%
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 1: 15th Ave NE \& NE 150th St


| Lane Group | EBL | $\rightarrow$ | EBR | WBL | $\leftarrow$ WBT |  | ${ }_{\text {NBL }}$ | $\uparrow$ NBT | NBR | SBL | $\frac{1}{*}$ SBT | $\stackrel{\downarrow}{\text { SBR }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | $\uparrow$ | 「 |  | $\uparrow$ | 「 | ${ }^{7}$ | $\hat{\beta}$ |  | ${ }^{7}$ | $\uparrow$ | F |
| Traffic Volume (vph) | 227 | 32 | 198 | 53 | 68 | 82 | 339 | 950 | 39 | 39 | 410 | 167 |
| Future Volume (vph) | 227 | 32 | 198 | 53 | 68 | 82 | 339 | 950 | 39 | 39 | 410 | 167 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 10 | 12 | 10 | 10 | 11 | 11 | 11 | 12 | 10 | 11 | 11 | 12 |
| Storage Length (ft) | 0 |  | 75 | 0 |  | 0 | 60 |  | 0 | 90 |  | 140 |
| Storage Lanes | 0 |  | 1 | 0 |  | 1 | 1 |  | 0 | 1 |  | 1 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  | 0.99 | 0.97 |  | 1.00 | 0.96 | 0.99 | 1.00 |  |  |  | 0.96 |
| Frt |  |  | 0.850 |  |  | 0.850 |  | 0.994 |  |  |  | 0.850 |
| Flt Protected |  | 0.958 |  |  | 0.979 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1785 | 1478 | 0 | 1763 | 1531 | 1711 | 1849 | 0 | 1711 | 1801 | 1583 |
| Flt Permitted |  | 0.660 |  |  | 0.628 |  | 0.463 |  |  | 0.119 |  |  |
| Satd. Flow (perm) | 0 | 1217 | 1428 | 0 | 1128 | 1476 | 827 | 1849 | 0 | 214 | 1801 | 1527 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  | 167 |  |  | 145 |  | 3 |  |  |  | 178 |
| Link Speed (mph) |  | 30 |  |  | 25 |  |  | 35 |  |  | 35 |  |
| Link Distance (ft) |  | 577 |  |  | 127 |  |  | 874 |  |  | 1332 |  |
| Travel Time (s) |  | 13.1 |  |  | 3.5 |  |  | 17.0 |  |  | 25.9 |  |
| Confl. Peds. (\#/hr) | 6 |  | 5 | 5 |  | 6 | 6 |  | 4 | 4 |  | 6 |
| Confl. Bikes (\#/hr) |  |  | 2 |  |  | 2 |  |  | 3 |  |  | 1 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Adj. Flow (vph) | 241 | 34 | 211 | 56 | 72 | 87 | 361 | 1011 | 41 | 41 | 436 | 178 |
| Shared Lane Trafic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 275 | 211 | 0 | 128 | 87 | 361 | 1052 | 0 | 41 | 436 | 178 |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | pm+pt | NA |  | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 4 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  | 4 | 4 |  | 4 | 2 |  |  | 6 |  | 6 |
| Detector Phase | 4 | 4 | 4 | , | 4 | 4 | 5 | 2 |  | 1 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 | 5.0 | 10.0 |  | 5.0 | 10.0 | 10.0 |
| Minimum Split (s) | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 12.0 | 21.0 |  | 12.0 | 23.0 | 23.0 |
| Total Split (s) | 29.0 | 29.0 | 29.0 | 29.0 | 29.0 | 29.0 | 18.0 | 49.0 |  | 12.0 | 43.0 | 43.0 |
| Total Split (\%) | 32.2\% | 32.2\% | 32.2\% | 32.2\% | 32.2\% | 32.2\% | 20.0\% | 54.4\% |  | 13.3\% | 47.8\% | 47.8\% |
| Maximum Green (s) | 24.0 | 24.0 | 24.0 | 24.0 | 24.0 | 24.0 | 13.0 | 44.0 |  | 7.0 | 38.0 | 38.0 |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) |  | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 |
| Lead/Lag |  |  |  |  |  |  | Lag | Lag |  | Lead | Lead | Lead |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes |  | Yes | Yes | Yes |
| Vehicle Extension (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 |
| Recall Mode | None | None | None | None | None | None | None | C-Max |  | None | C-Max | C-Max |
| Walk Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 |  |  | 7.0 | 7.0 |
| Flash Dont Walk (s) | 13.0 | 13.0 | 13.0 | 13.0 | 13.0 | 13.0 |  | 9.0 |  |  | 11.0 | 11.0 |
| Pedestrian Calls (\#/hr) | 2 | 2 | 2 | 2 | 2 | 2 |  | 0 |  |  | 5 | 5 |
| Act Effct Green (s) |  | 22.7 | 22.7 |  | 22.7 | 22.7 | 50.5 | 50.5 |  | 39.3 | 39.3 | 39.3 |


| Lane Group | ¢ EBL | $\rightarrow$ | EBR | WBL | $\leftarrow$ WBT |  | 4 | 4 NBT | NBR | ¢ SBL | t SBT | $\stackrel{\downarrow}{\text { SBR }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Actuated g/C Ratio |  | 0.25 | 0.25 |  | 0.25 | 0.25 | 0.56 | 0.56 |  | 0.44 | 0.44 | 0.44 |
| v/c Ratio |  | 0.90 | 0.44 |  | 0.45 | 0.18 | 0.61 | 1.01 |  | 0.22 | 0.55 | 0.23 |
| Control Delay |  | 64.7 | 10.4 |  | 33.6 | 1.8 | 23.6 | 55.1 |  | 18.2 | 22.7 | 3.5 |
| Queue Delay |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Delay |  | 64.7 | 10.4 |  | 33.6 | 1.8 | 23.6 | 55.1 |  | 18.2 | 22.7 | 3.5 |
| LOS |  | E | B |  | C | A | C | E |  | B | C | A |
| Approach Delay |  | 41.1 |  |  | 20.8 |  |  | 47.1 |  |  | 17.2 |  |
| Approach LOS |  | D |  |  | C |  |  | D |  |  | B |  |
| Queue Length 50th (ft) |  | 148 | 19 |  | 60 | 0 | 123 | $\sim 703$ |  | 13 | 184 | 0 |
| Queue Length 95th (ft) |  | \#288 | 77 |  | 115 | 9 | 198 | \#961 |  | 33 | 279 | 37 |
| Internal Link Dist (ft) |  | 497 |  |  | 47 |  |  | 794 |  |  | 1252 |  |
| Turn Bay Length (ft) |  |  | 75 |  |  |  | 60 |  |  | 90 |  | 140 |
| Base Capacity (vph) |  | 324 | 503 |  | 300 | 499 | 591 | 1038 |  | 209 | 786 | 767 |
| Starvation Cap Reductn |  | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 |
| Spillback Cap Reductn |  | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 |
| Storage Cap Reductn |  | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 |
| Reduced v/c Ratio |  | 0.85 | 0.42 |  | 0.43 | 0.17 | 0.61 | 1.01 |  | 0.20 | 0.55 | 0.23 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type: Other
Cycle Length: 90
Actuated Cycle Length: 90
Offset: $0(0 \%)$, Referenced to phase 2:NBTL and 6:SBTL, Start of Green
Natural Cycle: 100
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 1.01
Intersection Signal Delay: $36.9 \quad$ Intersection LOS: D
Intersection Capacity Utilization 92.8\% ICU Level of Service F
Analysis Period (min) 15
~ Volume exceeds capacity, queue is theoretically infinite.
Queue shown is maximum after two cycles.
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 2: 15th Ave NE \& NE 155th St


| Lane Group | - EBL | $\rightarrow$ | EBR | WBL | $\leftarrow$ WBT | WBR | ${ }_{\text {NBL }}$ | $\uparrow$ <br> NBT | $\stackrel{+}{\text { NBR }}$ | SBL | ¢ SBT | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | $\hat{\beta}$ |  | ${ }^{\text {\% }}$ | $\hat{i}$ |  | ${ }^{7}$ | $\hat{1}$ |  | ${ }^{7}$ | $\dagger$ |  |
| Traffic Volume (vph) | 194 | 568 | 62 | 52 | 370 | 59 | 181 | 523 | 118 | 31 | 107 | 69 |
| Future Volume (vph) | 194 | 568 | 62 | 52 | 370 | 59 | 181 | 523 | 118 | 31 | 107 | 69 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 11 | 11 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Storage Length (ft) | 110 |  | 0 | 100 |  | 0 | 105 |  | 0 | 160 |  | 0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length ( ft ) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 0.99 |  |
| Frt |  | 0.985 |  |  | 0.979 |  |  | 0.972 |  |  | 0.941 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1770 | 1769 | 0 | 1770 | 1817 | 0 | 1770 | 1803 | 0 | 1687 | 1656 | 0 |
| Flt Permitted | 0.340 |  |  | 0.190 |  |  | 0.636 |  |  | 0.178 |  |  |
| Satd. Flow (perm) | 632 | 1769 | 0 | 354 | 1817 | 0 | 1183 | 1803 | 0 | 316 | 1656 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 12 |  |  | 17 |  |  | 26 |  |  | 75 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 572 |  |  | 796 |  |  | 673 |  |  | 531 |  |
| Travel Time (s) |  | 13.0 |  |  | 18.1 |  |  | 15.3 |  |  | 12.1 |  |
| Confl. Peds. (\#/hr) | 3 |  | 3 | 3 |  | 3 | 1 |  | 2 | 2 |  | 1 |
| Confl. Bikes (\#hr) |  |  | 2 |  |  | 2 |  |  |  |  |  | 1 |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 7\% | 7\% | 7\% |
| Adj. Flow (vph) | 213 | 624 | 68 | 57 | 407 | 65 | 199 | 575 | 130 | 34 | 118 | 76 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 213 | 692 | 0 | 57 | 472 | 0 | 199 | 705 | 0 | 34 | 194 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 2 |  |  | 2 |  |  | 4 |  |  | 4 |  |
| Permitted Phases | 2 |  |  | 2 |  |  | 4 |  |  | 4 |  |  |
| Detector Phase | 2 | 2 |  | 2 | 2 |  | 4 | 4 |  | 4 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Minimum Split (s) | 24.0 | 24.0 |  | 24.0 | 24.0 |  | 24.0 | 24.0 |  | 24.0 | 24.0 |  |
| Total Split (s) | 26.0 | 26.0 |  | 26.0 | 26.0 |  | 29.0 | 29.0 |  | 29.0 | 29.0 |  |
| Total Split (\%) | 47.3\% | 47.3\% |  | 47.3\% | 47.3\% |  | 52.7\% | 52.7\% |  | 52.7\% | 52.7\% |  |
| Maximum Green (s) | 21.0 | 21.0 |  | 21.0 | 21.0 |  | 24.0 | 24.0 |  | 24.0 | 24.0 |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Recall Mode | None | None |  | None | None |  | None | None |  | None | None |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 12.0 | 12.0 |  | 12.0 | 12.0 |  | 12.0 | 12.0 |  | 12.0 | 12.0 |  |
| Pedestrian Calls (\#/hr) | 5 | 5 |  | 5 | 5 |  | 7 | 7 |  | 7 | 7 |  |
| Act Effct Green (s) | 21.1 | 21.1 |  | 21.1 | 21.1 |  | 22.5 | 22.5 |  | 22.5 | 22.5 |  |


| Lane Group | $\stackrel{4}{\text { EBL }}$ | $\rightarrow$ |  | WBL |  |  | NBL | 4 NBT | NBR | SBL | $\frac{1}{*}$ SBT | $\stackrel{ }{\text { ¢ }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Actuated g/C Ratio | 0.39 | 0.39 |  | 0.39 | 0.39 |  | 0.42 | 0.42 |  | 0.42 | 0.42 |  |
| v/c Ratio | 0.86 | 0.99 |  | 0.41 | 0.65 |  | 0.40 | 0.91 |  | 0.26 | 0.26 |  |
| Control Delay | 52.2 | 51.5 |  | 23.5 | 18.5 |  | 13.6 | 33.6 |  | 16.0 | 7.3 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 52.2 | 51.5 |  | 23.5 | 18.5 |  | 13.6 | 33.6 |  | 16.0 | 7.3 |  |
| LOS | D | D |  | C | B |  | B | C |  | B | A |  |
| Approach Delay |  | 51.6 |  |  | 19.0 |  |  | 29.2 |  |  | 8.6 |  |
| Approach LOS |  | D |  |  | B |  |  | C |  |  | A |  |
| Queue Length 50th (ft) | 63 | $\sim 222$ |  | 13 | 119 |  | 42 | 192 |  | 7 | 22 |  |
| Queue Length 95th (ft) | \#174 | \#427 |  | \#52 | 207 |  | 86 | \#389 |  | 26 | 55 |  |
| Internal Link Dist (ft) |  | 492 |  |  | 716 |  |  | 593 |  |  | 451 |  |
| Turn Bay Length ( t ) | 110 |  |  | 100 |  |  | 105 |  |  | 160 |  |  |
| Base Capacity (vph) | 248 | 702 |  | 139 | 724 |  | 531 | 824 |  | 141 | 785 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.86 | 0.99 |  | 0.41 | 0.65 |  | 0.37 | 0.86 |  | 0.24 | 0.25 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 55 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 53.6 |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Uncoordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.99 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 33.2 |  |  |  |  | Intersection LOS: C |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 93.4\% ICU Level of Service F |  |  |  |  |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| Splits and Phases: 3: 5th Ave NE \& NE 155th St |  |  |  |  |  |  |  |  |  |  |  |  |
| $\xrightarrow[\square]{\leftrightarrows}$ |  |  |  |  | 1404 |  |  |  |  |  |  |  |
| 26. |  |  |  |  | 298 |  |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 83.2 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS | F |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 243 | 76 | 61 | 5 | 13 | 5 | 73 | 581 | 6 | 5 | 115 | 57 |
| Future Vol, veh/h | 243 | 76 | 61 | 5 | 13 | 5 | 73 | 581 | 6 | 5 | 115 | 57 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.75 | 0.75 | 0.75 | 0.87 | 0.87 | 0.87 | 0.75 | 0.75 | 0.75 |
| Heavy Vehicles, \% | , |  | 1 | 5 | 5 | 5 | 0 | 0 | 0 | 1 | 1 | 1 |
| Mvmt Flow | 251 | 78 | 63 | 7 | 17 | 7 | 84 | 668 | 7 | 7 | 153 | 76 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | , |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 24.7 |  |  | 11.8 |  |  | 137.7 |  |  | 14.3 |  |  |
| HCM LOS | C |  |  | B |  |  | F |  |  | B |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $11 \%$ | $64 \%$ | $22 \%$ | $3 \%$ |
| Vol Thru, \% | $88 \%$ | $20 \%$ | $57 \%$ | $65 \%$ |
| Vol Right, \% | $1 \%$ | $16 \%$ | $22 \%$ | $32 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 660 | 380 | 23 | 177 |
| LT Vol | 73 | 243 | 5 | 5 |
| Through Vol | 581 | 76 | 13 | 115 |
| RT Vol | 6 | 61 | 5 | 57 |
| Lane Flow Rate | 759 | 392 | 31 | 236 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 1.23 | 0.702 | 0.064 | 0.411 |
| Departure Headway (Hd) | 5.838 | 6.948 | 8.192 | 6.684 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 622 | 525 | 440 | 543 |
| Service Time | 3.885 | 4.948 | 6.192 | 4.684 |
| HCM Lane V/C Ratio | 1.22 | 0.747 | 0.07 | 0.435 |
| HCM Control Delay | 137.7 | 24.7 | 11.8 | 14.3 |
| HCM Lane LOS | F | C | B | B |
| HCM 95th-tile Q | 27.8 | 5.5 | 0.2 | 2 |




| Approach | EB | WB | NB | SB |
| :--- | :--- | :--- | ---: | ---: |
| HCM Control Delay, s | 0.1 | 0.6 | 14.1 | 12.8 |
| HCM LOS |  |  | B | B |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 571 | 1386 | - | -1225 | - | - | 509 |  |
| HCM Lane V/C Ratio | 0.312 | 0.004 | - | -0.012 | - | -0.089 |  |  |
| HCM Control Delay (s) | 14.1 | 7.6 | 0 | - | 8 | 0 | -12.8 |  |
| HCM Lane LOS | B | A | A | - | A | A | - | B |
| HCM 95th \%tile Q(veh) | 1.3 | 0 | - | - | 0 | - | - | 0.3 |


| Lane Group | * | $\begin{aligned} & \rightarrow \\ & \text { EBT } \end{aligned}$ | EBR | WBL | ~ | W | $\begin{aligned} & 4 \\ & \text { NBL } \end{aligned}$ | ¢ | NBR | - | ¢ SBT | $\downarrow$ SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | $\uparrow$ |  |  | $\uparrow$ |  | ${ }^{7}$ | 1\% |  | ${ }^{7}$ | 中 ${ }^{\text {\% }}$ |  |
| Traffic Volume (vph) | 1 | 4 | 3 | 94 | 4 | 193 | 3 | 396 | 237 | 248 | 940 | 2 |
| Future Volume (vph) | 1 | 4 | 3 | 94 | 4 | 193 | 3 | 396 | 237 | 248 | 940 | 2 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 11 | 11 | 11 | 12 | 11 | 11 | 12 | 11 | 11 |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 45 |  | 0 | 80 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 |
| Ped Bike Factor |  | 0.99 |  |  | 0.98 |  |  | 0.99 |  | 0.99 | 1.00 |  |
| Frt |  | 0.949 |  |  | 0.910 |  |  | 0.944 |  |  |  |  |
| Flt Protected |  | 0.994 |  |  | 0.984 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1780 | 0 | 0 | 1528 | 0 | 1752 | 3152 | 0 | 1752 | 3387 | 0 |
| Flt Permitted |  | 0.994 |  |  | 0.984 |  | 0.188 |  |  | 0.384 |  |  |
| Satd. Flow (perm) | 0 | 1778 | 0 | 0 | 1525 | 0 | 347 | 3152 | 0 | 703 | 3387 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 3 |  |  | 82 |  |  | 129 |  |  |  |  |
| Link Speed (mph) |  | 10 |  |  | 30 |  |  | 35 |  |  | 35 |  |
| Link Distance (ft) |  | 100 |  |  | 1032 |  |  | 672 |  |  | 440 |  |
| Travel Time (s) |  | 6.8 |  |  | 23.5 |  |  | 13.1 |  |  | 8.6 |  |
| Confl. Peds. (\#/hr) | 6 |  | 4 | 4 |  | 6 | 24 |  | 7 | 7 |  | 24 |
| Confl. Bikes (\#/hr) |  |  |  |  |  | 1 |  |  |  |  |  | 1 |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Heavy Vehicles (\%) | 0\% | 0\% | 0\% | 6\% | 6\% | 6\% | 3\% | 3\% | 3\% | 3\% | 3\% | 3\% |
| Adj. Flow (vph) | 1 | 4 | 3 | 98 | 4 | 201 | 3 | 413 | 247 | 258 | 979 | 2 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 8 | 0 | 0 | 303 | 0 | 3 | 660 | 0 | 258 | 981 | 0 |
| Turn Type | Split | NA |  | Split | NA |  | pm+pt | NA |  | pm+pt | NA |  |
| Protected Phases | 4 | 4 |  | 3 | 3 |  | 1 | 6 |  | 5 | 2 |  |
| Permitted Phases |  |  |  |  |  |  | 6 |  |  | 2 |  |  |
| Detector Phase | 4 | 4 |  | 3 | 3 |  | 1 | 6 |  | 5 | 2 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 10.0 | 10.0 |  | 5.0 | 15.0 |  | 5.0 | 15.0 |  |
| Minimum Split (s) | 24.0 | 24.0 |  | 25.0 | 25.0 |  | 12.0 | 25.0 |  | 12.0 | 20.0 |  |
| Total Split (s) | 24.0 | 24.0 |  | 28.0 | 28.0 |  | 12.0 | 46.0 |  | 12.0 | 46.0 |  |
| Total Split (\%) | 21.8\% | 21.8\% |  | 25.5\% | 25.5\% |  | 10.9\% | 41.8\% |  | 10.9\% | 41.8\% |  |
| Maximum Green (s) | 19.0 | 19.0 |  | 23.0 | 23.0 |  | 7.0 | 41.0 |  | 7.0 | 41.0 |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) |  | 0.0 |  |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) |  | 5.0 |  |  | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Lead/Lag | Lag | Lag |  | Lead | Lead |  | Lead | Lead |  | Lag | Lag |  |
| Lead-Lag Optimize? | Yes | Yes |  | Yes | Yes |  | Yes | Yes |  | Yes | Yes |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None |  | None | C-Max |  | None | C-Max |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  |  | 7.0 |  |  | 7.0 |  |
| Flash Dont Walk (s) | 12.0 | 12.0 |  | 13.0 | 13.0 |  |  | 13.0 |  |  | 6.0 |  |
| Pedestrian Calls (\#/hr) | 8 | 8 |  | 4 | 4 |  |  | 7 |  |  | 14 |  |
| Act Effct Green (s) |  | 8.4 |  |  | 20.2 |  | 60.8 | 60.8 |  | 70.6 | 70.6 |  |



| Lane Group | ¢ EBL | $\rightarrow$ | EBR | WBL | $\bullet$ WBT | 4 WBR | 4 | $\uparrow$ <br> NBT | NBR | SBL | ¢ SBT | $\stackrel{\downarrow}{\text { SBR }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | $\uparrow$ | \% |  | $\uparrow$ | F | ${ }^{7}$ | $\hat{1}$ |  | ${ }^{*}$ | $\uparrow$ | F |
| Traffic Volume (vph) | 63 | 76 | 340 | 34 | 26 | 12 | 237 | 276 | 84 | 111 | 933 | 344 |
| Future Volume (vph) | 63 | 76 | 340 | 34 | 26 | 12 | 237 | 276 | 84 | 111 | 933 | 344 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 10 | 12 | 10 | 10 | 11 | 11 | 11 | 12 | 10 | 11 | 11 | 12 |
| Storage Length (ft) | 0 |  | 75 | 0 |  | 0 | 60 |  | 0 | 90 |  | 140 |
| Storage Lanes | 0 |  | 1 | 0 |  | 1 | 1 |  | 0 | 1 |  | 1 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  | 1.00 | 0.97 |  | 1.00 | 0.97 |  | 0.99 |  | 1.00 |  | 0.97 |
| Frt |  |  | 0.850 |  |  | 0.850 |  | 0.965 |  |  |  | 0.850 |
| Flt Protected |  | 0.978 |  |  | 0.973 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1822 | 1478 | 0 | 1144 | 994 | 1662 | 1736 | 0 | 1711 | 1801 | 1583 |
| FIt Permitted |  | 0.824 |  |  | 0.782 |  | 0.096 |  |  | 0.401 |  |  |
| Satd. Flow (perm) | 0 | 1532 | 1438 | 0 | 918 | 968 | 168 | 1736 | 0 | 721 | 1801 | 1530 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  | 278 |  |  | 145 |  | 26 |  |  |  | 195 |
| Link Speed (mph) |  | 30 |  |  | 25 |  |  | 35 |  |  | 35 |  |
| Link Distance (ft) |  | 577 |  |  | 127 |  |  | 874 |  |  | 1332 |  |
| Travel Time (s) |  | 13.1 |  |  | 3.5 |  |  | 17.0 |  |  | 25.9 |  |
| Confl. Peds. (\#/hr) | 2 |  | 1 | 1 |  | 2 | 5 |  | 1 | 1 |  | 5 |
| Confl. Bikes (\#hr) |  |  | 3 |  |  | 1 |  |  | 2 |  |  | 2 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 100\% | 0\% | 57\% | 5\% | 5\% | 5\% | 2\% | 2\% | 2\% |
| Adj. Flow (vph) | 67 | 81 | 362 | 36 | 28 | 13 | 252 | 294 | 89 | 118 | 993 | 366 |
| Shared Lane Trafic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 148 | 362 | 0 | 64 | 13 | 252 | 383 | 0 | 118 | 993 | 366 |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | pm+pt | NA |  | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 4 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  | 4 | 4 |  | 4 | 2 |  |  | 6 |  | 6 |
| Detector Phase | 4 | 4 | 4 | 4 | 4 | 4 | 5 | 2 |  | 1 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 | 5.0 | 10.0 |  | 5.0 | 10.0 | 10.0 |
| Minimum Split (s) | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 12.0 | 21.0 |  | 12.0 | 23.0 | 23.0 |
| Total Split (s) | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 15.0 | 53.0 |  | 12.0 | 50.0 | 50.0 |
| Total Split (\%) | 27.8\% | 27.8\% | 27.8\% | 27.8\% | 27.8\% | 27.8\% | 16.7\% | 58.9\% |  | 13.3\% | 55.6\% | 55.6\% |
| Maximum Green (s) | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 | 10.0 | 48.0 |  | 7.0 | 45.0 | 45.0 |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) |  | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 |
| Lead/Lag |  |  |  |  |  |  | Lag | Lag |  | Lead | Lead | Lead |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes |  | Yes | Yes | Yes |
| Vehicle Extension (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 |
| Recall Mode | None | None | None | None | None | None | None | C-Max |  | None | C-Max | C-Max |
| Walk Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 |  |  | 7.0 | 7.0 |
| Flash Dont Walk (s) | 13.0 | 13.0 | 13.0 | 13.0 | 13.0 | 13.0 |  | 9.0 |  |  | 11.0 | 11.0 |
| Pedestrian Calls (\#/hr) | 2 | 2 | 2 | 2 | 2 | 2 |  | 0 |  |  | 5 | 5 |



Area Type: Other
Cycle Length: 90
Actuated Cycle Length: 90
Offset: $0(0 \%)$, Referenced to phase 2:NBTL and 6:SBTL, Start of Green
Natural Cycle: 100
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 1.02
Intersection Signal Delay: 37.7
Intersection Capacity Utilization 95.5\%
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 2: 15th Ave NE \& NE 155th St


| Lane Group | t EBL | $\rightarrow \underset{\text { EBT }}{\rightarrow}$ | EBR | WBL | $\leftarrow$ WBT | WBR | ${ }_{\text {NBL }}$ | $\uparrow$ NBT | $\underset{\text { NBR }}{ }$ | SBL | $\downarrow$ SBT | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | $\dagger$ |  | ${ }^{7}$ | $\uparrow$ |  | ${ }^{7}$ | $\hat{F}$ |  | ${ }^{7}$ | $\dagger$ |  |
| Traffic Volume (vph) | 62 | 298 | 79 | 178 | 453 | 24 | 120 | 80 | 102 | 70 | 420 | 176 |
| Future Volume (vph) | 62 | 298 | 79 | 178 | 453 | 24 | 120 | 80 | 102 | 70 | 420 | 176 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 11 | 11 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Storage Length (ft) | 110 |  | 0 | 100 |  | 0 | 105 |  | 0 | 160 |  | 0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | 1.00 | 0.99 |  | 1.00 | 1.00 |  | 1.00 |  |  |  | 0.99 |  |
| Frt |  | 0.969 |  |  | 0.993 |  |  | 0.916 |  |  | 0.956 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1703 | 1670 | 0 | 1736 | 1812 | 0 | 1703 | 1642 | 0 | 1687 | 1686 | 0 |
| Flt Permitted | 0.295 |  |  | 0.420 |  |  | 0.223 |  |  | 0.637 |  |  |
| Satd. Flow (perm) | 527 | 1670 | 0 | 765 | 1812 | 0 | 399 | 1642 | 0 | 1131 | 1686 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 28 |  |  | 6 |  |  | 107 |  |  | 49 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 572 |  |  | 796 |  |  | 673 |  |  | 531 |  |
| Travel Time (s) |  | 13.0 |  |  | 18.1 |  |  | 15.3 |  |  | 12.1 |  |
| Confl. Peds. (\#/hr) | 5 |  | 4 | 4 |  | 5 | 2 |  |  |  |  | 2 |
| Confl. Bikes (\#hr) |  |  |  |  |  |  |  |  |  |  |  | 1 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles (\%) | 6\% | 6\% | 6\% | 4\% | 4\% | 4\% | 6\% | 6\% | 6\% | 7\% | 7\% | 7\% |
| Adj. Flow (vph) | 65 | 314 | 83 | 187 | 477 | 25 | 126 | 84 | 107 | 74 | 442 | 185 |
| Shared Lane Trafic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 65 | 397 | 0 | 187 | 502 | 0 | 126 | 191 | 0 | 74 | 627 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 2 |  |  | 2 |  |  | , |  |  | 4 |  |
| Permitted Phases | 2 |  |  | 2 |  |  | 4 |  |  | 4 |  |  |
| Detector Phase | 2 | 2 |  | 2 | 2 |  | 4 | 4 |  | 4 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Minimum Split (s) | 24.0 | 24.0 |  | 24.0 | 24.0 |  | 24.0 | 24.0 |  | 24.0 | 24.0 |  |
| Total Split (s) | 26.0 | 26.0 |  | 26.0 | 26.0 |  | 29.0 | 29.0 |  | 29.0 | 29.0 |  |
| Total Split (\%) | 47.3\% | 47.3\% |  | 47.3\% | 47.3\% |  | 52.7\% | 52.7\% |  | 52.7\% | 52.7\% |  |
| Maximum Green (s) | 21.0 | 21.0 |  | 21.0 | 21.0 |  | 24.0 | 24.0 |  | 24.0 | 24.0 |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Recall Mode | None | None |  | None | None |  | None | None |  | None | None |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 12.0 | 12.0 |  | 12.0 | 12.0 |  | 12.0 | 12.0 |  | 12.0 | 12.0 |  |
| Pedestrian Calls (\#/hr) | 5 | 5 |  | 5 | 5 |  | 7 | 7 |  | 7 | 7 |  |
| Act Effct Green (s) | 17.4 | 17.4 |  | 17.4 | 17.4 |  | 20.2 | 20.2 |  | 20.2 | 20.2 |  |


| Lane Group | ¢ EBL | $\rightarrow$ |  | WBL | - WBT |  | 4 | 4 NBT | NBR | SBL | $\frac{1}{*}$ SBT | ¢ SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Actuated g/C Ratio | 0.36 | 0.36 |  | 0.36 | 0.36 |  | 0.42 | 0.42 |  | 0.42 | 0.42 |  |
| v/c Ratio | 0.34 | 0.64 |  | 0.68 | 0.76 |  | 0.75 | 0.25 |  | 0.16 | 0.85 |  |
| Control Delay | 18.1 | 17.8 |  | 29.2 | 23.2 |  | 45.5 | 5.8 |  | 10.4 | 26.0 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 18.1 | 17.8 |  | 29.2 | 23.2 |  | 45.5 | 5.8 |  | 10.4 | 26.0 |  |
| LOS | B | B |  | C | C |  | D | A |  | B | C |  |
| Approach Delay |  | 17.9 |  |  | 24.8 |  |  | 21.6 |  |  | 24.4 |  |
| Approach LOS |  | B |  |  | C |  |  | C |  |  | C |  |
| Queue Length 50th (ft) | 14 | 93 |  | 48 | 133 |  | 32 | 15 |  | 14 | 157 |  |
| Queue Length 95th (ft) | 43 | 170 |  | \#132 | \#246 |  | \#114 | 47 |  | 35 | \#334 |  |
| Internal Link Dist (ft) |  | 492 |  |  | 716 |  |  | 593 |  |  | 451 |  |
| Turn Bay Length (ft) | 110 |  |  | 100 |  |  | 105 |  |  | 160 |  |  |
| Base Capacity (vph) | 241 | 780 |  | 351 | 834 |  | 209 | 911 |  | 592 | 907 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.27 | 0.51 |  | 0.53 | 0.60 |  | 0.60 | 0.21 |  | 0.13 | 0.69 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type: Other

Cycle Length: 55
Actuated Cycle Length: 48.2
Natural Cycle: 55
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.85
Intersection Signal Delay: 22.7
Intersection LOS: C
Intersection Capacity Utilization 86.6\% ICU Level of Service E
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

Splits and Phases: 3: 5th Ave NE \& NE 155th St


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 140.1 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\dagger$ |  |  | $\uparrow$ |  |  | * |  |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 230 | 33 | 118 | 31 | 45 | 13 | 84 | 166 | 1 | 3 | 311 | 156 |
| Future Vol, veh/h | 230 | 33 | 118 | 31 | 45 | 13 | 84 | 166 | 1 | 3 | 311 | 156 |
| Peak Hour Factor | 0.64 | 0.64 | 0.64 | 0.63 | 0.63 | 0.63 | 0.63 | 0.63 | 0.63 | 0.73 | 0.73 | 0.73 |
| Heavy Vehicles, \% | - |  | 1 | 5 | 5 | 5 | 0 | 0 | 0 | 1 | 1 | 1 |
| Mvmt Flow | 359 | 52 | 184 | 49 | 71 | 21 | 133 | 263 | 2 | 4 | 426 | 214 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right |  |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 165.4 |  |  | 20.6 |  |  | 52.7 |  |  | 97.1 |  |  |
| HCM LOS | F |  |  | C |  |  | F |  |  | F |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $33 \%$ | $60 \%$ | $35 \%$ | $1 \%$ |
| Vol Thru, \% | $66 \%$ | $9 \%$ | $51 \%$ | $66 \%$ |
| Vol Right, \% | $0 \%$ | $31 \%$ | $15 \%$ | $33 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 251 | 381 | 89 | 470 |
| LT Vol | 84 | 230 | 31 | 3 |
| Through Vol | 166 | 33 | 45 | 311 |
| RT Vol | 1 | 118 | 13 | 156 |
| Lane Flow Rate | 398 | 595 | 141 | 644 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.88 | 1.272 | 0.364 | 1.352 |
| Departure Headway (Hd) | 9.545 | 8.475 | 11.269 | 8.35 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 382 | 435 | 322 | 438 |
| Service Time | 7.545 | 6.475 | 9.269 | 6.35 |
| HCM Lane V/C Ratio | 1.042 | 1.368 | 0.438 | 1.47 |
| HCM Control Delay | 52.7 | 165.4 | 20.6 | 197.1 |
| HCM Lane LOS | F | F | C | F |
| HCM 95th-tile Q | 8.7 | 23.2 | 1.6 | 27.1 |


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 1.8 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | 1 |  |  | $\uparrow$ | M |  |
| Traffic Vol, veh/h | 278 | 42 | 23 | 314 | 27 | 23 |
| Future Vol, veh/h | 278 | 42 | 23 | 314 | 27 | 23 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 12 | 5 |
| Sign Control F | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# |  | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 64 | 64 | 78 | 78 | 57 | 57 |
| Heavy Vehicles, \% | 1 | 1 | 5 | 5 | 7 | 7 |
| Mumt Flow | 434 | 66 | 29 | 403 | 47 | 40 |
| Major/Minor M | Major1 |  | Major2 |  | Minor1 |  |
| Conflicting Flow All | 0 | 0 | 500 | 0 | 940 | 472 |
| Stage 1 | - | - | - | - | 467 | - |
| Stage 2 | - | - | - | - | 473 | - |
| Critical Hdwy | - |  | 4.15 | - | 6.47 | 6.27 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.47 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.47 | - |
| Follow-up Hdwy | - | - | 2.245 | - | 3.563 | 3.363 |
| Pot Cap-1 Maneuver | - | - | 1049 | - | 287 | 582 |
| Stage 1 | - | - | - | . | 621 | . |
| Stage 2 | - | - | - | - | 617 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1049 | - | 274 | 579 |
| Mov Cap-2 Maneuver | - |  |  | - | 274 | - |
| Stage 1 |  |  | - | - | 621 | - |
| Stage 2 | - | - | - | - | 588 |  |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0.6 | 18.1 |
| HCM LOS |  |  | C |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 362 | - | -1049 | - |  |
| HCM Lane V/C Ratio | 0.242 | - | -0.028 | - |  |
| HCM Control Delay (s) | 18.1 | - | - | 8.5 | 0 |
| HCM Lane LOS | C | - | - | A | A |
| HCM 95th \%tile Q(veh) | 0.9 | - | - | 0.1 | - |


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 3 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\uparrow$ | $\dagger$ |  | \% |  |
| Traffic Vol, veh/h | 186 | 314 | 318 | 23 | 6 | 52 |
| Future Vol, veh/h | 186 | 314 | 318 | 23 | 6 | 52 |
| Conflicting Peds, \#/hr | 15 | 0 | 0 | 15 | 5 | 5 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | \# | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 64 | 64 | 78 | 78 | 92 | 92 |
| Heavy Vehicles, \% | , | 1 | 5 |  | 2 | 2 |
| Mvmt Flow | 291 | 491 | 408 | 29 | 7 | 57 |


| Major/Minor | Major1 | Major2 |  | Minor2 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Conflicting Flow All | 452 | 0 | - | 0 | 1516 | 443 |
| $\quad$ Stage 1 | - | - | - | - | 438 | - |
| $\quad$ Stage 2 | - | - | - | -1078 | - |  |
| Critical Hdwy | 4.11 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.209 | - | - | -3.518 | 3.318 |  |
| Pot Cap-1 Maneuver | 1114 | - | - | - | 131 | 615 |
| $\quad$ Stage 1 | - | - | - | - | 651 | - |
| Stage 2 | - | - | - | - | 327 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1098 | - | - | - | 81 | 603 |
| Mov Cap-2 Maneuver | - | - | - | - | 81 | - |
| Stage 1 | - | - | - | - | 408 | - |


| Approach | EB | WB | SB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 3.5 | 0 | 17 |
| HCM LOS |  |  | C |


| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1098 | - | - | -362 |
| HCM Lane V/C Ratio | 0.265 | - | - | -0.174 |
| HCM Control Delay (s) | 9.5 | 0 | - | -17 |
| HCM Lane LOS | A | A | - | - |
| Co |  |  |  |  |
| HCM 95th \%tile Q(veh) | 1.1 | - | - | - |
| C | 0.6 |  |  |  |


| Lane Group | - EBL | $\rightarrow$ | EBR | WBL | $\leftarrow$ WBT | 4 WBR | 4 | 4 NBT | NBR |  | ¢ SBT | $\stackrel{\downarrow}{\text { SBR }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | \$ |  |  | $\uparrow$ |  | ${ }^{7}$ | 个 ${ }^{2}$ |  | ${ }^{7}$ | 个t |  |
| Traffic Volume (vph) | 5 | 0 | 11 | 196 | 1 | 258 | 6 | 1231 | 174 | 158 | 568 | 8 |
| Future Volume (vph) | 5 | 0 | 11 | 196 | 1 | 258 | 6 | 1231 | 174 | 158 | 568 | 8 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width ( ft ) | 12 | 12 | 12 | 11 | 11 | 11 | 12 | 11 | 11 | 12 | 11 | 11 |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 45 |  | 0 | 80 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (tt) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 |
| Ped Bike Factor |  | 0.99 |  |  | 0.99 |  |  | 1.00 |  |  | 1.00 |  |
| Frt |  | 0.907 |  |  | 0.923 |  |  | 0.981 |  |  | 0.998 |  |
| Flt Protected |  | 0.985 |  |  | 0.979 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1679 | 0 | 0 | 1608 | 0 | 1787 | 3377 | 0 | 1770 | 3411 | 0 |
| Flt Permitted |  | 0.985 |  |  | 0.979 |  | 0.334 |  |  | 0.084 |  |  |
| Satd. Flow (perm) | 0 | 1677 | 0 | 0 | 1605 | 0 | 628 | 3377 | 0 | 156 | 3411 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 169 |  |  | 55 |  |  | 16 |  |  | 1 |  |
| Link Speed (mph) |  | 10 |  |  | 30 |  |  | 35 |  |  | 35 |  |
| Link Distance (ft) |  | 100 |  |  | 1031 |  |  | 672 |  |  | 440 |  |
| Travel Time (s) |  | 6.8 |  |  | 23.4 |  |  | 13.1 |  |  | 8.6 |  |
| Confl. Peds. (\#/hr) | 5 |  | 2 | 2 |  | 5 | 12 |  | 4 | 4 |  | 12 |
| Confl. Bikes (\#/hr) |  |  |  |  |  | 1 |  |  |  |  |  | 1 |
| Peak Hour Factor | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Heavy Vehicles (\%) | 0\% | 0\% | 0\% | 2\% | 2\% | 2\% | 1\% | 1\% | 1\% | 2\% | 2\% | 2\% |
| Adj. Flow (vph) | 5 | 0 | 11 | 200 | 1 | 263 | 6 | 1256 | 178 | 161 | 580 | 8 |
| Shared Lane Trafic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 16 | 0 | 0 | 464 | 0 | 6 | 1434 | 0 | 161 | 588 | 0 |
| Turn Type | Split | NA |  | Split | NA |  | pm+pt | NA |  | pm+pt | NA |  |
| Protected Phases | 4 | 4 |  | 3 | 3 |  | 1 | 6 |  | 5 | 2 |  |
| Permitted Phases |  |  |  |  |  |  | 6 |  |  | 2 |  |  |
| Detector Phase | 4 | 4 |  | 3 | 3 |  | 1 | 6 |  | 5 | 2 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 10.0 | 10.0 |  | 5.0 | 15.0 |  | 5.0 | 15.0 |  |
| Minimum Split (s) | 24.0 | 24.0 |  | 25.0 | 25.0 |  | 12.0 | 25.0 |  | 12.0 | 20.0 |  |
| Total Split (s) | 24.0 | 24.0 |  | 29.0 | 29.0 |  | 12.0 | 45.0 |  | 12.0 | 45.0 |  |
| Total Split (\%) | 21.8\% | 21.8\% |  | 26.4\% | 26.4\% |  | 10.9\% | 40.9\% |  | 10.9\% | 40.9\% |  |
| Maximum Green (s) | 19.0 | 19.0 |  | 24.0 | 24.0 |  | 7.0 | 40.0 |  | 7.0 | 40.0 |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) |  | 0.0 |  |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) |  | 5.0 |  |  | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Lead/Lag | Lag | Lag |  | Lead | Lead |  | Lead | Lead |  | Lag | Lag |  |
| Lead-Lag Optimize? | Yes | Yes |  | Yes | Yes |  | Yes | Yes |  | Yes | Yes |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None |  | None | C-Max |  | None | C-Max |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  |  | 7.0 |  |  | 7.0 |  |
| Flash Dont Walk (s) | 12.0 | 12.0 |  | 13.0 | 13.0 |  |  | 13.0 |  |  | 6.0 |  |
| Pedestrian Calls (\#/hr) | 8 | 8 |  | 4 | 4 |  |  | 7 |  |  | 14 |  |
| Act Effct Green (s) |  | 8.2 |  |  | 24.0 |  | 55.0 | 55.0 |  | 64.7 | 64.7 |  |


| Lane Group | EBL | $\rightarrow$ |  | WBL | $\leftarrow$ WBT |  | 4 | 4 <br> NBT |  |  | $\stackrel{\downarrow}{\text { ¢ }}$ | $\stackrel{ }{*}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Actuated g/C Ratio |  | 0.07 |  |  | 0.22 |  | 0.50 | 0.50 |  | 0.59 | 0.59 |  |
| v/c Ratio |  | 0.06 |  |  | 1.18 |  | 0.02 | 0.85 |  | 0.83 | 0.29 |  |
| Control Delay |  | 0.4 |  |  | 139.1 |  | 19.2 | 31.1 |  | 50.7 | 6.0 |  |
| Queue Delay |  | 0.0 |  |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay |  | 0.4 |  |  | 139.1 |  | 19.2 | 31.1 |  | 50.7 | 6.0 |  |
| LOS |  | A |  |  | F |  | B | C |  | D | A |  |
| Approach Delay |  | 0.4 |  |  | 139.1 |  |  | 31.1 |  |  | 15.6 |  |
| Approach LOS |  | A |  |  | F |  |  | C |  |  | B |  |
| Queue Length 50th (ft) |  | 0 |  |  | ~362 |  | 2 | 454 |  | 53 | 50 |  |
| Queue Length 95th (ft) |  | 0 |  |  | \#567 |  | 12 | \#770 |  | m\#189 | m141 |  |
| Internal Link Dist (ft) |  | 20 |  |  | 951 |  |  | 592 |  |  | 360 |  |
| Turn Bay Length (t) |  |  |  |  |  |  | 45 |  |  | 80 |  |  |
| Base Capacity (vph) |  | 429 |  |  | 393 |  | 388 | 1696 |  | 194 | 2007 |  |
| Starvation Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio |  | 0.04 |  |  | 1.18 |  | 0.02 | 0.85 |  | 0.83 | 0.29 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type: Other
Cycle Length: 110
Actuated Cycle Length: 110
Offset: 14 (13\%), Referenced to phase 2:SBTL and 6:NBTL, Start of Green
Natural Cycle: 150
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 1.18
Intersection Signal Delay: $45.3 \quad$ Intersection LOS: D
Intersection Capacity Utilization 94.6\% ICU Level of Service F
Analysis Period (min) 15
~ Volume exceeds capacity, queue is theoretically infinite.
Queue shown is maximum after two cycles.
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
$m$ Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 1: 15th Ave NE \& NE 150th St


| Lane Group | EBL | $\rightarrow$ | EBR | WBL | $\leftarrow$ WBT |  | ${ }_{\text {NBL }}$ | 4 NBT | NBR | SBL | $\stackrel{\downarrow}{\downarrow}$ | $\stackrel{\downarrow}{\text { SBR }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | $\uparrow$ | \% |  | $\uparrow$ | 7 | ${ }_{1}$ | $\stackrel{\rightharpoonup}{1}$ |  | ${ }^{*}$ | $\uparrow$ | F |
| Traffic Volume (vph) | 227 | 49 | 233 | 122 | 130 | 88 | 419 | 963 | 69 | 41 | 416 | 167 |
| Future Volume (vph) | 227 | 49 | 233 | 122 | 130 | 88 | 419 | 963 | 69 | 41 | 416 | 167 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 10 | 12 | 10 | 10 | 11 | 11 | 11 | 12 | 10 | 11 | 11 | 12 |
| Storage Length (ft) | 0 |  | 75 | 0 |  | 0 | 60 |  | 0 | 90 |  | 140 |
| Storage Lanes | 0 |  | 1 | 0 |  | 1 | 1 |  | 0 | 1 |  | 1 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  | 0.99 | 0.96 |  | 1.00 | 0.96 | 0.99 | 1.00 |  |  |  | 0.96 |
| Frt |  |  | 0.850 |  |  | 0.850 |  | 0.990 |  |  |  | 0.850 |
| Flt Protected |  | 0.960 |  |  | 0.976 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1788 | 1478 | 0 | 1757 | 1531 | 1711 | 1840 | 0 | 1711 | 1801 | 1583 |
| Flt Permitted |  | 0.444 |  |  | 0.491 |  | 0.385 |  |  | 0.118 |  |  |
| Satd. Flow (perm) | 0 | 821 | 1425 | 0 | 881 | 1471 | 687 | 1840 | 0 | 212 | 1801 | 1522 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  | 158 |  |  | 119 |  | 5 |  |  |  | 136 |
| Link Speed (mph) |  | 30 |  |  | 25 |  |  | 35 |  |  | 35 |  |
| Link Distance (ft) |  | 577 |  |  | 127 |  |  | 874 |  |  | 1332 |  |
| Travel Time (s) |  | 13.1 |  |  | 3.5 |  |  | 17.0 |  |  | 25.9 |  |
| Confl. Peds. (\#/hr) | 6 |  | 5 | 5 |  | 6 | 6 |  | 4 | 4 |  | 6 |
| Confl. Bikes (\#/hr) |  |  | 2 |  |  | 2 |  |  | 3 |  |  | 1 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Adj. Flow (vph) | 241 | 52 | 248 | 130 | 138 | 94 | 446 | 1024 | 73 | 44 | 443 | 178 |
| Shared Lane Trafic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 293 | 248 | 0 | 268 | 94 | 446 | 1097 | 0 | 44 | 443 | 178 |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | pm+pt | NA |  | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 4 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  | 4 | 4 |  | 4 | 2 |  |  | 6 |  | 6 |
| Detector Phase | 4 | 4 | 4 | 4 | 4 | 4 | 5 | 2 |  | 1 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 | 5.0 | 10.0 |  | 5.0 | 10.0 | 10.0 |
| Minimum Split (s) | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 12.0 | 21.0 |  | 12.0 | 23.0 | 23.0 |
| Total Split (s) | 38.0 | 38.0 | 38.0 | 38.0 | 38.0 | 38.0 | 27.0 | 60.0 |  | 12.0 | 45.0 | 45.0 |
| Total Split (\%) | 34.5\% | 34.5\% | 34.5\% | 34.5\% | 34.5\% | 34.5\% | 24.5\% | 54.5\% |  | 10.9\% | 40.9\% | 40.9\% |
| Maximum Green (s) | 33.0 | 33.0 | 33.0 | 33.0 | 33.0 | 33.0 | 22.0 | 55.0 |  | 7.0 | 40.0 | 40.0 |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) |  | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 |
| Lead/Lag |  |  |  |  |  |  | Lag | Lag |  | Lead | Lead | Lead |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes |  | Yes | Yes | Yes |
| Vehicle Extension (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 |
| Recall Mode | None | None | None | None | None | None | None | C-Max |  | None | C-Max | C-Max |
| Walk Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 |  |  | 7.0 | 7.0 |
| Flash Dont Walk (s) | 13.0 | 13.0 | 13.0 | 13.0 | 13.0 | 13.0 |  | 9.0 |  |  | 11.0 | 11.0 |
| Pedestrian Calls (\#/hr) | 2 | 2 | 2 | 2 | 2 | 2 |  | 0 |  |  | 5 | 5 |
| Act Effct Green (s) |  | 33.0 | 33.0 |  | 33.0 | 33.0 | 57.9 | 57.9 |  | 40.0 | 40.0 | 40.0 |


| Lane Group | ¢ EBL | $\rightarrow$ | EBR | WBL | - | 4 WBR | 4 | $\dagger$ <br> NBT | NBR | SBL | ¢ SBT | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Actuated g/C Ratio |  | 0.30 | 0.30 |  | 0.30 | 0.30 | 0.53 | 0.53 |  | 0.36 | 0.36 | 0.36 |
| $\mathrm{v} / \mathrm{c}$ Ratio |  | 1.19 | 0.46 |  | 1.02 | 0.18 | 0.79 | 1.13 |  | 0.28 | 0.68 | 0.28 |
| Control Delay |  | 154.7 | 14.5 |  | 99.0 | 3.7 | 22.7 | 84.8 |  | 27.4 | 35.8 | 8.3 |
| Queue Delay |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Delay |  | 154.7 | 14.5 |  | 99.0 | 3.7 | 22.7 | 84.8 |  | 27.4 | 35.8 | 8.3 |
| LOS |  | F | B |  | F | A | C | F |  | C | D | A |
| Approach Delay |  | 90.4 |  |  | 74.3 |  |  | 66.8 |  |  | 27.9 |  |
| Approach LOS |  | F |  |  | E |  |  | E |  |  | C |  |
| Queue Length 50th (ft) |  | $\sim 250$ | 47 |  | ~194 | 0 | 91 | ~902 |  | 20 | 261 | 19 |
| Queue Length 95th (ft) |  | \#421 | 121 |  | \#365 | 25 | m164 | m\#1070 |  | 45 | 377 | 68 |
| Internal Link Dist (ft) |  | 497 |  |  | 47 |  |  | 794 |  |  | 1252 |  |
| Turn Bay Length ( ft ) |  |  | 75 |  |  |  | 60 |  |  | 90 |  | 140 |
| Base Capacity (vph) |  | 246 | 538 |  | 264 | 524 | 566 | 970 |  | 172 | 654 | 640 |
| Starvation Cap Reductn |  | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 |
| Spillback Cap Reductn |  | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 |
| Storage Cap Reductn |  | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 |
| Reduced v/c Ratio |  | 1.19 | 0.46 |  | 1.02 | 0.18 | 0.79 | 1.13 |  | 0.26 | 0.68 | 0.28 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type: Other
Cycle Length: 110
Actuated Cycle Length: 110
Offset: $0(0 \%)$, Referenced to phase 2:NBTL and 6:SBTL, Start of Green
Natural Cycle: 150
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 1.19
Intersection Signal Delay: $63.5 \quad$ Intersection LOS: E
Intersection Capacity Utilization 105.3\% ICU Level of Service G
Analysis Period (min) 15
~ Volume exceeds capacity, queue is theoretically infinite.
Queue shown is maximum after two cycles.
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
$m$ Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 2: 15th Ave NE \& NE 155th St


| Lane Group | 4 EBL | $\underset{\text { EBT }}{\rightarrow}$ | EBR | WBL | ↔- WBT | WBR | 4 | $\uparrow$ NBT | NBR | SBL | $\stackrel{\downarrow}{\dagger}$ | ¢ SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ |  |  | ${ }^{4}$ | $\dagger$ |  | ${ }^{4}$ | $\stackrel{\rightharpoonup}{1}$ |  | ${ }^{7}$ | $\hat{}$ |  |
| Traffic Volume (vph) | 194 | 586 | 62 | 139 | 417 | 62 | 181 | 523 | 150 | 32 | 107 | 69 |
| Future Volume (vph) | 194 | 586 | 62 | 139 | 417 | 62 | 181 | 523 | 150 | 32 | 107 | 69 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 11 | 11 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Storage Length (ft) | 110 |  | 0 | 100 |  | 0 | 105 |  | 0 | 160 |  | 0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 0.99 |  | 1.00 | 0.99 |  |
| Frt |  | 0.986 |  |  | 0.981 |  |  | 0.967 |  |  | 0.941 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1770 | 1771 | 0 | 1770 | 1821 | 0 | 1770 | 1792 | 0 | 1687 | 1656 | 0 |
| Flt Permitted | 0.275 |  |  | 0.190 |  |  | 0.636 |  |  | 0.173 |  |  |
| Satd. Flow (perm) | 511 | 1771 | 0 | 354 | 1821 | 0 | 1183 | 1792 | 0 | 307 | 1656 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 11 |  |  | 16 |  |  | 33 |  |  | 75 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 572 |  |  | 796 |  |  | 673 |  |  | 531 |  |
| Travel Time (s) |  | 13.0 |  |  | 18.1 |  |  | 15.3 |  |  | 12.1 |  |
| Confl. Peds. (\#/hr) | 3 |  | 3 | 3 |  | 3 | 1 |  | 2 | 2 |  | 1 |
| Confl. Bikes (\#hr) |  |  | 2 |  |  | 2 |  |  |  |  |  | 1 |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 7\% | 7\% | 7\% |
| Adj. Flow (vph) | 213 | 644 | 68 | 153 | 458 | 68 | 199 | 575 | 165 | 35 | 118 | 76 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 213 | 712 | 0 | 153 | 526 | 0 | 199 | 740 | 0 | 35 | 194 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 2 |  |  | 2 |  |  | 4 |  |  | 4 |  |
| Permitted Phases | 2 |  |  | 2 |  |  | 4 |  |  |  |  |  |
| Detector Phase | 2 | 2 |  | 2 | 2 |  | 4 | 4 |  | 4 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Minimum Split (s) | 24.0 | 24.0 |  | 24.0 | 24.0 |  | 24.0 | 24.0 |  | 24.0 | 24.0 |  |
| Total Split (s) | 26.0 | 26.0 |  | 26.0 | 26.0 |  | 29.0 | 29.0 |  | 29.0 | 29.0 |  |
| Total Split (\%) | 47.3\% | 47.3\% |  | 47.3\% | 47.3\% |  | 52.7\% | 52.7\% |  | 52.7\% | 52.7\% |  |
| Maximum Green (s) | 21.0 | 21.0 |  | 21.0 | 21.0 |  | 24.0 | 24.0 |  | 24.0 | 24.0 |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Recall Mode | None | None |  | None | None |  | None | None |  | None | None |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 12.0 | 12.0 |  | 12.0 | 12.0 |  | 12.0 | 12.0 |  | 12.0 | 12.0 |  |
| Pedestrian Calls (\#/hr) | 5 | 5 |  | 5 | 5 |  | 7 | 7 |  | 7 | 7 |  |
| Act Effct Green (s) | 21.0 | 21.0 |  | 21.0 | 21.0 |  | 23.1 | 23.1 |  | 23.1 | 23.1 |  |


| Lane Group | ¢ EBL | $\rightarrow$ |  | WBL | $*$ WBT |  | 4 | 4 NBT | NBR | SBL | $\frac{1}{*}$ SBT | $\stackrel{\downarrow}{\text { SBR }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Actuated g/C Ratio | 0.39 | 0.39 |  | 0.39 | 0.39 |  | 0.43 | 0.43 |  | 0.43 | 0.43 |  |
| v/c Ratio | 1.08 | 1.02 |  | 1.12 | 0.73 |  | 0.39 | 0.95 |  | 0.27 | 0.26 |  |
| Control Delay | 110.1 | 61.8 |  | 137.8 | 22.0 |  | 13.5 | 38.6 |  | 16.5 | 7.2 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 110.1 | 61.8 |  | 137.8 | 22.0 |  | 13.5 | 38.6 |  | 16.5 | 7.2 |  |
| LOS | F | E |  | F | C |  | B | D |  | B | A |  |
| Approach Delay |  | 72.9 |  |  | 48.1 |  |  | 33.2 |  |  | 8.7 |  |
| Approach LOS |  | E |  |  | D |  |  | C |  |  | A |  |
| Queue Length 50th (ft) | $\sim 82$ | $\sim 261$ |  | $\sim 61$ | 139 |  | 42 | 207 |  | 7 | 22 |  |
| Queue Length 95th (ft) | \#190 | \#444 |  | \#155 | \#278 |  | 86 | \#418 |  | 27 | 55 |  |
| Internal Link Dist (tt) |  | 492 |  |  | 716 |  |  | 593 |  |  | 451 |  |
| Turn Bay Length (ft) | 110 |  |  | 100 |  |  | 105 |  |  | 160 |  |  |
| Base Capacity (vph) | 198 | 695 |  | 137 | 717 |  | 525 | 813 |  | 135 | 776 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 1.08 | 1.02 |  | 1.12 | 0.73 |  | 0.38 | 0.91 |  | 0.26 | 0.25 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type: Other
Cycle Length: 55
Actuated Cycle Length: 54.1
Natural Cycle: 90
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 1.12
Intersection Signal Delay: $48.1 \quad$ Intersection LOS: D
Intersection Capacity Utilization 99.9\% ICU Level of Service F
Analysis Period (min) 15
~ Volume exceeds capacity, queue is theoretically infinite.
Queue shown is maximum after two cycles.
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 3: 5th Ave NE \& NE 155th St


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 94.5 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | $\uparrow$ |  |  | \$ |  |  | \$ |  |
| Traffic Vol, veh/h | 244 | 77 | 92 | 5 | 13 | 5 | 85 | 581 | 6 | 5 | 115 | 56 |
| Future Vol, veh/h | 244 | 77 | 92 | 5 | 13 | 5 | 85 | 581 | 6 | 5 | 115 | 56 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.75 | 0.75 | 0.75 | 0.87 | 0.87 | 0.87 | 0.75 | 0.75 | 0.75 |
| Heavy Vehicles, \% | 1 | 1 | 1 | 5 | 5 | 5 | 0 | 0 | 0 | 1 | 1 | 1 |
| Mvmt Flow | 252 | 79 | 95 | 7 | 17 | 7 | 98 | 668 | 7 | 7 | 153 | 75 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 28.7 |  |  | 12 |  |  | 158.2 |  |  | 14.7 |  |  |
| HCM LOS | D |  |  | B |  |  | F |  |  | B |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $13 \%$ | $59 \%$ | $22 \%$ | $3 \%$ |
| Vol Thru, \% | $86 \%$ | $19 \%$ | $57 \%$ | $65 \%$ |
| Vol Right, \% | $1 \%$ | $22 \%$ | $22 \%$ | $32 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 672 | 413 | 23 | 176 |
| LT Vol | 85 | 244 | 5 | 5 |
| Through Vol | 581 | 77 | 13 | 115 |
| RT Vol | 6 | 92 | 5 | 56 |
| Lane Flow Rate | 772 | 426 | 31 | 235 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 1.28 | 0.758 | 0.065 | 0.417 |
| Departure Headway (Hd) | 5.964 | 6.995 | 8.436 | 6.892 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 610 | 519 | 427 | 526 |
| Service Time | 4.016 | 4.995 | 6.436 | 4.892 |
| HCM Lane V/C Ratio | 1.266 | 0.821 | 0.073 | 0.447 |
| HCM Control Delay | 158.2 | 28.7 | 12 | 14.7 |
| HCM Lane LOS | F | D | B | B |
| HCM 95th-tile Q | 30.4 | 6.6 | 0.2 | 2 |


|  |  | Intersection |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 3.5 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | 1 |  |  | $\uparrow$ | M |  |
| Traffic Vol, veh/h | 275 | 32 | 10 | 126 | 46 | 71 |
| Future Vol, veh/h | 275 | 32 | 10 | 126 | 46 | 71 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 2 | 4 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# |  |  | - | 0 | 0 |  |
| Grade, \% | 0 | - | - | 0 | 0 |  |
| Peak Hour Factor | 78 | 78 | 66 | 66 | 64 | 64 |
| Heavy Vehicles, \% | 2 | 2 | 3 | 3 | 2 | 2 |
| Mvmt Flow | 353 | 41 | 15 | 191 | 72 | 111 |


| Major/Minor | Major1 | Major2 |  |  | Minor1 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | :---: |
| Conflicting Flow All | 0 | 0 | 394 | 0 | 597 | 378 |  |
| $\quad$ Stage 1 | - | - | - | - | 374 | - |  |
| Stage 2 | - | - | - | - | 223 | - |  |
| Critical Hdwy | - | - | 4.13 | - | 6.42 | 6.22 |  |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |  |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |  |
| Follow-up Hdwy | - | - | 2.227 | -3.518 | 3.318 |  |  |
| Pot Cap-1 Maneuver | - | - | 1159 | - | 466 | 669 |  |
| Stage 1 | - | - | - | - | 696 | - |  |
| Stage 2 | - | - | - | - | 814 | - |  |
| Platoon blocked, \% | - | - |  | - |  |  |  |
| Mov Cap-1 Maneuver | - | - | 1159 | - | 459 | 666 |  |
| Mov Cap-2 Maneuver | - | - | - | - | 459 | - |  |
| Stage 1 | - | - | - | - | 696 | - |  |
| Stage 2 | - | - | - | - | 801 | - |  |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0.6 | 14.4 |
| HCM LOS |  |  | B |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 566 | - | -1159 | - |  |
| HCM Lane V/C Ratio | 0.323 | - | -0.013 | - |  |
| HCM Control Delay (s) | 14.4 | - | - | 8.1 | 0 |
| HCM Lane LOS | B | - | - | A | A |
| HCM 95th \%tile Q(veh) | 1.4 | - | - | 0 | - |


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 5.4 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\uparrow$ | $\stackrel{\text { F }}{ }$ |  | M |  |
| Traffic Vol, veh/h | 106 | 277 | 161 | 11 | 30 | 248 |
| Future Vol, veh/h | 106 | 277 | 161 | 11 | 30 | 248 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - |  | - | - | 0 | - |
| Veh in Median Storage, \# | \# | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 78 | 78 | 66 | 66 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 3 |  | 2 | 2 |
| Mvmt Flow | 136 | 355 | 244 | 17 | 33 | 270 |


| Major/Minor | Major1 | Major2 |  |  |  |  |
| :--- | ---: | :--- | ---: | :--- | ---: | ---: |
| Conflicting Flow All | 261 | 0 | - | 0 | 880 | 253 |
| $\quad$ Stage 1 | - | - | - | - | 253 | - |
| Stage 2 | - | - | - | - | 627 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | -3.518 | 3.318 |  |
| Pot Cap-1 Maneuver | 1303 | - | - | - | 318 | 786 |
| $\quad$ Stage 1 | - | - | - | - | 789 | - |
| Stage 2 | - | - | - | - | 532 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1303 | - | - | - | 277 | 786 |
| Mov Cap-2 Maneuver | - | - | - | - | 277 | - |
| Stage 1 | - | - | - | - | 686 | - |
| Stage 2 | - | - | - | - | 532 | - |


| Approach | EB | WB | SB |
| :--- | :--- | ---: | ---: |
| HCM Control Delay, s | 2.2 | 0 | 15.1 |
| HCM LOS |  |  | C |


| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1303 | - | - | -656 |
| HCM Lane V/C Ratio | 0.104 | - | - | -0.461 |
| HCM Control Delay (s) | 8.1 | 0 | - | -15.1 |
| HCM Lane LOS | A | A | - | - |
| HCM 95th \%tile Q(veh) | 0.3 | - | - | - |
| C | 2.4 |  |  |  |


| Lane Group | \% EBL | $\underset{\text { EBT }}{\rightarrow}$ | EBR | WBL | $\leftarrow$ WBT | WBR | 4 | ¢ NBT | $\stackrel{+}{\text { NBR }}$ |  | ¢ SBT | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | \$ |  |  | \$ |  | \% | 个 ${ }^{2}$ |  | ${ }^{*}$ | $\uparrow{ }^{+}$ |  |
| Trafic Volume (vph) | 5 | 0 | 11 | 196 | 1 | 258 | 6 | 1231 | 174 | 158 | 568 | 8 |
| Future Volume (vph) | 5 | 0 | 11 | 196 | 1 | 258 | 6 | 1231 | 174 | 158 | 568 | 8 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 11 | 11 | 11 | 12 | 11 | 11 | 12 | 11 | 11 |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 45 |  | 0 | 80 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (tt) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 |
| Ped Bike Factor |  | 0.99 |  |  | 0.99 |  |  | 1.00 |  |  | 1.00 |  |
| Frt |  | 0.907 |  |  | 0.923 |  |  | 0.981 |  |  | 0.998 |  |
| FIt Protected |  | 0.985 |  |  | 0.979 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1679 | 0 | 0 | 1608 | 0 | 1787 | 3377 | 0 | 1770 | 3411 | 0 |
| FIt Permitted |  | 0.985 |  |  | 0.979 |  | 0.334 |  |  | 0.084 |  |  |
| Satd. Flow (perm) | 0 | 1677 | 0 | 0 | 1605 | 0 | 628 | 3377 | 0 | 156 | 3411 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 169 |  |  | 55 |  |  | 16 |  |  | 1 |  |
| Link Speed (mph) |  | 10 |  |  | 30 |  |  | 35 |  |  | 35 |  |
| Link Distance (ft) |  | 100 |  |  | 1031 |  |  | 672 |  |  | 440 |  |
| Travel Time (s) |  | 6.8 |  |  | 23.4 |  |  | 13.1 |  |  | 8.6 |  |
| Confl. Peds. (\#/hr) | 5 |  | 2 | 2 |  | 5 | 12 |  | 4 | 4 |  | 12 |
| Confl. Bikes (\#/hr) |  |  |  |  |  | 1 |  |  |  |  |  | 1 |
| Peak Hour Factor | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Heavy Vehicles (\%) | 0\% | 0\% | 0\% | 2\% | 2\% | 2\% | 1\% | 1\% | 1\% | 2\% | 2\% | 2\% |
| Adj. Flow (vph) | 5 | 0 | 11 | 200 | 1 | 263 | 6 | 1256 | 178 | 161 | 580 | 8 |
| Shared Lane Trafic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 16 | 0 | 0 | 464 | 0 | 6 | 1434 | 0 | 161 | 588 | 0 |
| Turn Type | Split | NA |  | Split | NA |  | pm+pt | NA |  | pm+pt | NA |  |
| Protected Phases | 4 | 4 |  | 3 | 3 |  | 1 | 6 |  | 5 | 2 |  |
| Permitted Phases |  |  |  |  |  |  | 6 |  |  | 2 |  |  |
| Detector Phase | 4 | 4 |  | 3 | 3 |  | 1 | 6 |  | 5 | 2 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 10.0 | 10.0 |  | 5.0 | 15.0 |  | 5.0 | 15.0 |  |
| Minimum Split (s) | 24.0 | 24.0 |  | 25.0 | 25.0 |  | 12.0 | 25.0 |  | 12.0 | 20.0 |  |
| Total Split (s) | 24.0 | 24.0 |  | 29.0 | 29.0 |  | 12.0 | 45.0 |  | 12.0 | 45.0 |  |
| Total Split (\%) | 21.8\% | 21.8\% |  | 26.4\% | 26.4\% |  | 10.9\% | 40.9\% |  | 10.9\% | 40.9\% |  |
| Maximum Green (s) | 19.0 | 19.0 |  | 24.0 | 24.0 |  | 7.0 | 40.0 |  | 7.0 | 40.0 |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) |  | 0.0 |  |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) |  | 5.0 |  |  | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Lead/Lag | Lag | Lag |  | Lead | Lead |  | Lead | Lead |  | Lag | Lag |  |
| Lead-Lag Optimize? | Yes | Yes |  | Yes | Yes |  | Yes | Yes |  | Yes | Yes |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None |  | None | C-Max |  | None | C-Max |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  |  | 7.0 |  |  | 7.0 |  |
| Flash Dont Walk (s) | 12.0 | 12.0 |  | 13.0 | 13.0 |  |  | 13.0 |  |  | 6.0 |  |
| Pedestrian Calls (\#/hr) | 8 | 8 |  | 4 | 4 |  |  | 7 |  |  | 14 |  |
| Act Effct Green (s) |  | 8.2 |  |  | 24.0 |  | 55.0 | 55.0 |  | 64.7 | 64.7 |  |


| Lane Group | ¢ EBL | $\rightarrow$ |  | WBL |  |  | 4 NBL | 4 NBT |  | SBL | ¢ SBT | ¢ SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Actuated g/C Ratio |  | 0.07 |  |  | 0.22 |  | 0.50 | 0.50 |  | 0.59 | 0.59 |  |
| v/c Ratio |  | 0.06 |  |  | 1.18 |  | 0.02 | 0.85 |  | 0.83 | 0.29 |  |
| Control Delay |  | 0.4 |  |  | 139.1 |  | 19.2 | 31.1 |  | 51.9 | 5.9 |  |
| Queue Delay |  | 0.0 |  |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay |  | 0.4 |  |  | 139.1 |  | 19.2 | 31.1 |  | 51.9 | 5.9 |  |
| LOS |  | A |  |  | F |  | B | C |  | D | A |  |
| Approach Delay |  | 0.4 |  |  | 139.1 |  |  | 31.1 |  |  | 15.8 |  |
| Approach LOS |  | A |  |  | F |  |  | C |  |  | B |  |
| Queue Length 50th (ft) |  | 0 |  |  | $\sim 362$ |  | 2 | 454 |  | 53 | 48 |  |
| Queue Length 95th (ft) |  | 0 |  |  | \#567 |  | 12 | \#770 |  | m\#211 | 152 |  |
| Internal Link Dist (ft) |  | 20 |  |  | 951 |  |  | 592 |  |  | 360 |  |
| Turn Bay Length (ft) |  |  |  |  |  |  | 45 |  |  | 80 |  |  |
| Base Capacity (vph) |  | 429 |  |  | 393 |  | 388 | 1696 |  | 194 | 2007 |  |
| Starvation Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio |  | 0.04 |  |  | 1.18 |  | 0.02 | 0.85 |  | 0.83 | 0.29 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type: Other
Cycle Length: 110
Actuated Cycle Length: 110
Offset: 14 (13\%), Referenced to phase 2:SBTL and 6:NBTL, Start of Green
Natural Cycle: 150
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 1.18
Intersection Signal Delay: $45.4 \quad$ Intersection LOS: D
Intersection Capacity Utilization 94.6\% ICU Level of Service F
Analysis Period (min) 15
~ Volume exceeds capacity, queue is theoretically infinite.
Queue shown is maximum after two cycles.
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
$m$ Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 1: 15th Ave NE \& NE 150th St


|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


| Lane Group | 4 EBL | $\rightarrow$ |  | WBL | - WBT |  | ${ }_{\text {NBL }}$ | $\uparrow$ <br> NBT | NBR | SBL | $\downarrow$ SBT | ¢ SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Actuated g/C Ratio | 0.24 | 0.16 |  | 0.24 | 0.16 |  | 0.56 | 0.56 |  | 0.40 | 0.40 | 0.40 |
| $\mathrm{v} / \mathrm{c}$ Ratio | 1.14 | 0.72 |  | 0.70 | 0.80 |  | 0.74 | 1.07 |  | 0.28 | 0.61 | 0.26 |
| Control Delay | 138.7 | 26.5 |  | 51.9 | 59.5 |  | 18.4 | 59.3 |  | 25.6 | 31.1 | 7.3 |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Delay | 138.7 | 26.5 |  | 51.9 | 59.5 |  | 18.4 | 59.3 |  | 25.6 | 31.1 | 7.3 |
| LOS | F | C |  | D | E |  | B | E |  | C | C | A |
| Approach Delay |  | 76.5 |  |  | 56.8 |  |  | 47.5 |  |  | 24.3 |  |
| Approach LOS |  | E |  |  | E |  |  | D |  |  | C |  |
| Queue Length 50th (ft) | ~163 | 70 |  | 71 | 140 |  | 87 | $\sim 874$ |  | 19 | 247 | 16 |
| Queue Length 95th (ft) | \#269 | 168 |  | \#135 | \#242 |  | m156 | \#1057 |  | 43 | 366 | 63 |
| Internal Link Dist (ft) |  | 497 |  |  | 47 |  |  | 794 |  |  | 1252 |  |
| Turn Bay Length (ft) | 115 |  |  | 40 |  |  | 60 |  |  | 90 |  | 140 |
| Base Capacity (vph) | 212 | 443 |  | 186 | 324 |  | 599 | 1025 |  | 172 | 724 | 695 |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Reduced v/c Ratio | 1.14 | 0.68 |  | 0.70 | 0.72 |  | 0.74 | 1.07 |  | 0.26 | 0.61 | 0.26 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

ntersection Summary
Area Type: Other
Cycle Length: 110
Actuated Cycle Length: 110
Offset: $0(0 \%)$, Referenced to phase 2:NBTL and 6:SBTL, Start of Green
Natural Cycle: 150
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 1.14
Intersection Signal Delay: $48.7 \quad$ Intersection LOS: D
Intersection Capacity Utilization 100.7\% ICU Level of Service G
Analysis Period (min) 15
~ Volume exceeds capacity, queue is theoretically infinite.
Queue shown is maximum after two cycles.
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
$m$ Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 2: 15th Ave NE \& NE 155th St


| Lane Group | - EBL | $\rightarrow$ | EBR | WBL | $\leftarrow$ WBT | 4 WBR | ${ }_{\text {NBL }}$ | $\uparrow$ NBT | NBR |  | ¢ SBT | $\stackrel{\downarrow}{\text { SBR }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ |  | ${ }^{1}$ | $\stackrel{\text { F }}{ }$ |  | ${ }^{7}$ | $\uparrow$ |  | ${ }^{7}$ | $\uparrow$ |  |
| Trafic Volume (vph) | 194 | 586 | 62 | 139 | 417 | 62 | 181 | 523 | 150 | 32 | 107 | 69 |
| Future Volume (vph) | 194 | 586 | 62 | 139 | 417 | 62 | 181 | 523 | 150 | 32 | 107 | 69 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 11 | 11 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Storage Length (ft) | 110 |  | 0 | 100 |  | 0 | 105 |  | 0 | 160 |  | 0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 0.99 |  | 1.00 | 0.99 |  |
| Frt |  | 0.986 |  |  | 0.981 |  |  | 0.967 |  |  | 0.941 |  |
| FIt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1770 | 1771 | 0 | 1770 | 1821 | 0 | 1770 | 1792 | 0 | 1687 | 1656 | 0 |
| FIt Permitted | 0.275 |  |  | 0.190 |  |  | 0.636 |  |  | 0.173 |  |  |
| Satd. Flow (perm) | 511 | 1771 | 0 | 354 | 1821 | 0 | 1183 | 1792 | 0 | 307 | 1656 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 11 |  |  | 16 |  |  | 33 |  |  | 75 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 572 |  |  | 796 |  |  | 673 |  |  | 531 |  |
| Travel Time (s) |  | 13.0 |  |  | 18.1 |  |  | 15.3 |  |  | 12.1 |  |
| Confl. Peds. (\#/hr) | 3 |  | 3 | 3 |  | 3 | 1 |  | 2 | 2 |  | 1 |
| Confl. Bikes (\#/hr) |  |  | 2 |  |  | 2 |  |  |  |  |  | 1 |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 7\% | 7\% | 7\% |
| Adj. Flow (vph) | 213 | 644 | 68 | 153 | 458 | 68 | 199 | 575 | 165 | 35 | 118 | 76 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 213 | 712 | 0 | 153 | 526 | 0 | 199 | 740 | 0 | 35 | 194 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 2 |  |  | 2 |  |  | 4 |  |  | 4 |  |
| Permitted Phases | 2 |  |  | 2 |  |  | 4 |  |  | 4 |  |  |
| Detector Phase | 2 | 2 |  | 2 | 2 |  | 4 | 4 |  | 4 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Minimum Split (s) | 24.0 | 24.0 |  | 24.0 | 24.0 |  | 24.0 | 24.0 |  | 24.0 | 24.0 |  |
| Total Split (s) | 26.0 | 26.0 |  | 26.0 | 26.0 |  | 29.0 | 29.0 |  | 29.0 | 29.0 |  |
| Total Split (\%) | 47.3\% | 47.3\% |  | 47.3\% | 47.3\% |  | 52.7\% | 52.7\% |  | 52.7\% | 52.7\% |  |
| Maximum Green (s) | 21.0 | 21.0 |  | 21.0 | 21.0 |  | 24.0 | 24.0 |  | 24.0 | 24.0 |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Recall Mode | None | None |  | None | None |  | None | None |  | None | None |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 12.0 | 12.0 |  | 12.0 | 12.0 |  | 12.0 | 12.0 |  | 12.0 | 12.0 |  |
| Pedestrian Calls (\#/hr) | 5 | 5 |  | 5 | 5 |  | 7 | 7 |  | 7 | 7 |  |
| Act Effct Green (s) | 21.0 | 21.0 |  | 21.0 | 21.0 |  | 23.1 | 23.1 |  | 23.1 | 23.1 |  |



|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


| Lane Group | $\begin{aligned} & \wedge \\ & \text { EBL } \end{aligned}$ | $\rightarrow$ | EBR | WBL | $\Perp$ WBT | $4$ <br> WBR | $\begin{aligned} & 4 \\ & \text { NBL } \end{aligned}$ | ¢ ${ }_{\text {NBT }}$ | N | SBL | $\stackrel{1}{\text { ¢ }}$ | ¢ SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total Delay |  | 42.3 |  |  | 12.5 |  |  | 27.3 |  |  | 6.9 |  |
| LOS |  | D |  |  | B |  |  | C |  |  | A |  |
| Approach Delay |  | 42.3 |  |  | 12.5 |  |  | 27.3 |  |  | 6.9 |  |
| Approach LOS |  | D |  |  | B |  |  | C |  |  | A |  |
| Queue Length 50th (ft) |  | 137 |  |  | 6 |  |  | 221 |  |  | 32 |  |
| Queue Length 95th (ft) |  | \#295 |  |  | 18 |  |  | \#412 |  |  | 50 |  |
| Internal Link Dist (ft) |  | 1257 |  |  | 565 |  |  | 357 |  |  | 339 |  |
| Turn Bay Length (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) |  | 510 |  |  | 543 |  |  | 977 |  |  | 993 |  |
| Starvation Cap Reductn |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Spillback Cap Reductn |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Storage Cap Reductn |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Reduced v/c Ratio |  | 0.84 |  |  | 0.06 |  |  | 0.79 |  |  | 0.24 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

## Area Type: Other

Cycle Length: 60
Actuated Cycle Length: 56.4
Natural Cycle: 65
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.89
Intersection Signal Delay: 28.1
Intersection LOS: C
Intersection Capacity Utilization 90.2\% ICU Level of Service E
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 4: 25th Ave NE \& NE 150th St


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 3.5 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | 1 |  |  | $\uparrow$ | M |  |
| Traffic Vol, veh/h | 275 | 32 | 10 | 126 | 46 | 71 |
| Future Vol, veh/h | 275 | 32 | 10 | 126 | 46 | 71 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 2 | 4 |
| Sign Control F | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | \# 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 |  |  | 0 | 0 |  |
| Peak Hour Factor | 78 | 78 | 66 | 66 | 64 | 64 |
| Heavy Vehicles, \% | 2 | 2 | 3 | 3 | 2 | 2 |
| Mumt Flow | 353 | 41 | 15 | 191 | 72 | 111 |


| Major/Minor | Major1 | Major2 | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 394 | 597 | 378 |
| Stage 1 | - | - - | - 374 | - |
| Stage 2 | - | - - | - 223 | - |
| Critical Hdwy | - | 4.13 | - 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - - | - 5.42 | - |
| Critical Hdwy Stg 2 | - | - - | - 5.42 | - |
| Follow-up Hdwy | - | - 2.227 | - 3.518 | 3.318 |
| Pot Cap-1 Maneuver | - | 1159 | - 466 | 669 |
| Stage 1 | - | - - | - 696 | - |
| Stage 2 | - | - - | - 814 | - |
| Platoon blocked, \% | - | - | - |  |
| Mov Cap-1 Maneuver | - | 1159 | - 459 | 666 |
| Mov Cap-2 Maneuver | - | - - | - 459 | - |
| Stage 1 | - | - - | - 696 | - |
| Stage 2 | - | - - | - 801 |  |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0.6 | 14.4 |
| HCM LOS |  |  | B |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 566 | - | -1159 | - |  |
| HCM Lane V/C Ratio | 0.323 | - | -0.013 | - |  |
| HCM Control Delay (s) | 14.4 | - | - | 8.1 | 0 |
| HCM Lane LOS | B | - | - | A | A |
| HCM 95th \%tile Q(veh) | 1.4 | - | - | 0 | - |


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 5.4 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\uparrow$ | $\dagger$ |  | M |  |
| Traffic Vol, veh/h | 106 | 277 | 161 | 11 | 30 | 248 |
| Future Vol, veh/h | 106 | 277 | 161 | 11 | 30 | 248 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized |  | None | - | None | , | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | \# | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 78 | 78 | 66 | 66 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 3 |  | 2 | 2 |
| Mvmt Flow | 136 | 355 | 244 | 17 | 33 | 270 |


| Major/Minor | Major1 | Major2 |  |  |  |  |
| :--- | ---: | :--- | ---: | :--- | ---: | ---: |
| Conflicting Flow All | 261 | 0 | - | 0 | 880 | 253 |
| $\quad$ Stage 1 | - | - | - | - | 253 | - |
| Stage 2 | - | - | - | - | 627 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | -3.518 | 3.318 |  |
| Pot Cap-1 Maneuver | 1303 | - | - | - | 318 | 786 |
| $\quad$ Stage 1 | - | - | - | - | 789 | - |
| Stage 2 | - | - | - | - | 532 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1303 | - | - | - | 277 | 786 |
| Mov Cap-2 Maneuver | - | - | - | - | 277 | - |
| Stage 1 | - | - | - | - | 686 | - |
| Stage 2 | - | - | - | - | 532 | - |


| Approach | EB | WB | SB |
| :--- | :--- | ---: | ---: |
| HCM Control Delay, s | 2.2 | 0 | 15.1 |
| HCM LOS |  |  | C |


| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1303 | - | - | -656 |
| HCM Lane V/C Ratio | 0.104 | - | - | -0.461 |
| HCM Control Delay (s) | 8.1 | 0 | - | -15.1 |
| HCM Lane LOS | A | A | - | - |
| HCM 95th \%tile Q(veh) | 0.3 | - | - | - |
| C | 2.4 |  |  |  |

# APPENDIX C Detailed Trip Generation Calculations 

DSHS Fircrest School: Existing Site - Trip Generation Estimates

| Proposed Uses | ITE | ITE Equation / Rate | Daily <br> Trips | AM Peak Hour Trips |  |  |  | PM Peak Hour Trips |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | LU Code |  |  | ITE Equation / Rate | In | Out | Total | ITE Equation / Rate | In | Out | Total |
| Nursing Home | 620 | 3.06 trips/bed | 370 | 0.14 trips/bed | $\begin{gathered} \hline 72 \% \\ 12 \end{gathered}$ | $\begin{gathered} 28 \% \\ 5 \end{gathered}$ | 17 | 0.14 trips/bed | $\begin{gathered} \hline 33 \% \\ 6 \end{gathered}$ | $\begin{gathered} \hline 67 \% \\ 11 \end{gathered}$ | 17 |
| Assisted Living | 254 | 2.60 trips/bed | 420 | 0.18 trips/bed | $\begin{gathered} \hline 60 \% \\ 17 \end{gathered}$ | $\begin{gathered} 40 \% \\ 12 \end{gathered}$ | 29 | 0.24 trips/bed | $\begin{gathered} \hline 39 \% \\ 15 \end{gathered}$ | $\begin{gathered} \hline 61 \% \\ 23 \end{gathered}$ | 38 |
| Single-Tenant Office | 715 | 13.07 trips/1,000 sf | 640 | $T=1.89(X)-7.67$ | $\begin{gathered} \hline 89 \% \\ 76 \end{gathered}$ | $\begin{gathered} \hline 11 \% \\ 9 \end{gathered}$ | 85 | $T=1.72(X)+7.89$ | $\begin{gathered} \hline 15 \% \\ 14 \end{gathered}$ | $\begin{gathered} 85 \% \\ 78 \end{gathered}$ | 92 |
| Off-Leash Dog Area | N/A | $\begin{gathered} 27.59 \text { trips } / 1,000 \text { sf } \\ \text { (assumes 10xPM) } \end{gathered}$ | 40 | 2.76 trips $/ 1,000 \mathrm{sf}$ (assumes same as PM) | $\begin{gathered} 56 \% \\ 2 \end{gathered}$ | $\begin{gathered} 44 \% \\ 2 \end{gathered}$ | 4 | 2.76 trips/acre1,000 sf * | $\begin{gathered} 56 \% \\ 2 \end{gathered}$ | $\begin{gathered} 44 \% \\ 2 \end{gathered}$ | 4 |
| Total for Existing Uses |  |  | 1,470 |  | 107 | 28 | 135 |  | 37 | 114 | 151 |

*Rate from Off-Leash Dog Area(s) at the Chambers Creek Properties, Heffron Transportation, Inc., November 14, 2006, [Weekday PM peak hour counts/observations at 3 OLAs (Grandview, Marymoor, and Magnuson)
DSHS Fircrest School: No Action - Trip Generation Estimates (TRANSIT ADJUSTED)

| Proposed Uses | $\begin{gathered} \text { ITE } \\ \text { LU Code } \end{gathered}$ | ITE Equation / Rate | $\begin{aligned} & \hline \text { Daily } \\ & \text { Trips } \end{aligned}$ | AM Peak Hour Trips |  |  |  | PM Peak Hour Trips |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | ITE Equation / Rate | In | Out | Total | ITE Equation / Rate | In | Out | Total |
| Nursing Home | 620 | 3.06 trips/bed | 350 | 0.14 trips/bed | $\begin{gathered} \hline 72 \% \\ 12 \end{gathered}$ | $\begin{gathered} 28 \% \\ 4 \end{gathered}$ | 16 | 0.14 trips/bed | $\begin{gathered} \hline 33 \% \\ 6 \end{gathered}$ | $\begin{gathered} 67 \% \\ 10 \end{gathered}$ | 16 |
| Assisted Living | 254 | 2.60 trips/bed | 390 | 0.18 trips/bed | $\begin{gathered} \hline 60 \% \\ 16 \end{gathered}$ | $\begin{gathered} 40 \% \\ 11 \end{gathered}$ | 27 | 0.24 trips/bed | $\begin{gathered} \hline 39 \% \\ 14 \end{gathered}$ | $\begin{gathered} \hline 61 \% \\ 22 \end{gathered}$ | 36 |
| Single-Tenant Office | 715 | 13.07 trips/1,000 sf | 1,110 | $T=1.89(X)-7.67$ | $\begin{array}{r} 89 \% \\ 135 \end{array}$ | $\begin{gathered} \hline 11 \% \\ 17 \end{gathered}$ | 152 | $T=1.72(X)+7.89$ | $\begin{gathered} \hline 15 \% \\ 23 \end{gathered}$ | $\begin{array}{r} \hline 85 \% \\ 130 \end{array}$ | 153 |
| Off-Leash Dog Area | N/A | 27.59 trips/1,000 sf | 40 | 2.76 trips/1,000 sf | $\begin{gathered} 56 \% \\ 2 \end{gathered}$ | $\begin{gathered} 44 \% \\ 2 \end{gathered}$ | 4 | 2.76 trips/acre1,000 sf * | $\begin{gathered} 56 \% \\ 2 \end{gathered}$ | $\begin{gathered} 44 \% \\ 2 \end{gathered}$ | 4 |
| Total for Fully Occupied Existing Uses |  |  | 1,890 |  | 165 | 34 | 199 |  | 45 | 164 | 209 |

Transit

DSHS Fircrest School: Proposed Master Plan - Trip Generation Estimates (TRANSIT ADJUSTED)

|  | ITE |  | Daily | AM Peak H | ur Trip |  |  | PM Peak H | r Trip |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Proposed Uses | LU Code | ITE Equation / Rate | Trips | ITE Equation / Rate | In | Out | Total | ITE Equation / Rate | In | Out | Total |
| Nursing Home | 620 | 3.06 trips/bed | 350 | 0.14 trips/bed | $\begin{array}{\|c\|} \hline 72 \% \\ 12 \end{array}$ | $\begin{array}{\|c\|} \hline 28 \% \\ 4 \end{array}$ | 16 | 0.14 trips/bed | $\begin{array}{\|c\|} \hline 33 \% \\ 5 \end{array}$ | $\begin{gathered} \hline 67 \% \\ 11 \\ \hline \end{gathered}$ | 16 |
| Single-Tenant Office | 715 | 13.07 trips/1,000 sf | 1110 | $T=1.89(X)-7.67$ | $\begin{array}{\|r} \hline 89 \% \\ 135 \\ \hline \end{array}$ | $\begin{array}{\|c} \hline 11 \% \\ 17 \\ \hline \end{array}$ | 152 | $T=1.72(X)+7.89$ | $\begin{gathered} \hline 15 \% \\ 23 \\ \hline \end{gathered}$ | $\begin{array}{r} \hline 85 \% \\ 130 \\ \hline \end{array}$ | 153 |
| Behavioral Health Hospital | 610 | 10.77 trips/1,000 sf | 530 | $\operatorname{Ln}(\mathrm{T})=0.60 \operatorname{Ln}(X)+2.52$ | $\begin{array}{\|c\|} \hline 67 \% \\ 84 \\ \hline \end{array}$ | $\begin{array}{\|c\|} \hline 33 \% \\ 41 \end{array}$ | 125 | $\operatorname{Ln}(T)=0.64 \operatorname{Ln}(X)+2.27$ | $\begin{array}{\|c} \hline 35 \% \\ 40 \end{array}$ | $\begin{gathered} \hline 65 \% \\ 74 \end{gathered}$ | 114 |
| Assisted Living | 254 | 2.60 trips/bed | 370 | 0.18 trips/bed | $\begin{array}{\|c} \hline 60 \% \\ 16 \end{array}$ | $\begin{array}{\|c} \hline 40 \% \\ 10 \end{array}$ | 26 | 0.24 trips/bed | $\begin{array}{\|c\|} \hline 39 \% \\ 13 \end{array}$ | $\begin{gathered} \hline 61 \% \\ 21 \\ \hline \end{gathered}$ | 34 |
| General Office | 710 | $\operatorname{Ln}(T)=0.87 \operatorname{Ln}(X)+3.05$ | 310 | $\operatorname{Ln}(T)=0.86 \operatorname{Ln}(X)+1.16$ | $\begin{gathered} \hline 88 \% \\ 40 \\ \hline \end{gathered}$ | $\begin{array}{\|c} \hline 12 \% \\ 5 \\ \hline \end{array}$ | 45 | $\operatorname{Ln}(T)=0.83 \operatorname{Ln}(X)+1.29$ | $\begin{array}{\|c\|} \hline 17 \% \\ 8 \end{array}$ | $\begin{gathered} 83 \% \\ 39 \end{gathered}$ | 47 |
| Day Care Center | 565 | 47.62 trips/1,000 sf | 110 | 11.00 trips/1,000 sf | $\begin{gathered} \hline 53 \% \\ 14 \end{gathered}$ | $\begin{array}{\|c} \hline 47 \% \\ 12 \\ \hline \end{array}$ | 26 | 11.12 trips/1,000 sf | $\begin{array}{\|c} \hline 47 \% \\ 12 \end{array}$ | $\begin{gathered} \hline 53 \% \\ 14 \end{gathered}$ | 26 |
| Medical/Dental Office | 720 | 36.00 trips/1,000 sf | 2,880 | $\operatorname{Ln}(T)=0.90 \operatorname{Ln}(X)+1.34$ | $\begin{array}{r} \hline 79 \% \\ 155 \end{array}$ | $\begin{gathered} \hline 21 \% \\ 41 \\ \hline \end{gathered}$ | 196 | $T=4.07(X)-3.17$ | $\begin{gathered} \hline 30 \% \\ 97 \end{gathered}$ | $\begin{array}{r} \hline 70 \% \\ 225 \\ \hline \end{array}$ | 322 |
| Clinic | 630 | 37.60 trips/1,000 sf | 0 | 2.75 trips/1,000 sf | $\begin{gathered} 81 \% \\ 0 \end{gathered}$ | $\begin{array}{\|c} \hline 19 \% \\ 0 \end{array}$ | 0 | 3.69 trips/1,000 sf | $\begin{array}{\|c} \hline 30 \% \\ 0 \end{array}$ |  | 0 |
| Total for Retained and Proposed New Uses |  |  | 5,660 |  | 456 | 130 | 586 |  | 198 | 514 | 712 |
| Transit trip estimates |  |  | 361 |  |  |  | 37 |  |  |  | 45 |
| Net Change for Total Site |  |  | 3,770 |  | 291 | 96 | 387 |  | 153 | 350 | 503 |
| Allocation for DSHS Elements |  |  | 470 |  | 82 | 38 | 120 |  | 36 | 122 | 108 |
| Allocation for Development by Others |  |  | 3,300 |  | 209 | 58 | 267 |  | 117 | 278 | 395 |


[^0]:    1 City of Shoreline, August 2018.
    ${ }^{2}$ City of Shoreline, Appendix E of the 2022 Engineering Development Manual, Effective March 1, 2022.
    3 Email communications, K. Dedinsky - City of Shoreline Traffic Engineer, March 2022.
    4 PLN22-0190 - MDP Review $1523015^{\text {th }}$ Ave NE - Fircrest School Master Development, Cory Johnson, April 12, 2023.
    5 MS Teams meeting, June 26, 2023.
    ${ }^{6}$ Email communications, A. Bumgarner - City of Shoreline Traffic Engineer, June 2023.
    7 ITE, What a Transportation Professional Needs to Know About Counts and Studies during a Pandemic, July 2020.
    8 Kittelson \& Associates, Estimating Traffic Volumes Under COVID-19 Pandemic Conditions, April 2, 2020.
    9 City of Shoreline, Zoning 2021 Land Use Zoning Map, July 2, 2021.
    10 DSHS website (https://www.dshs.wa.gov/dda/consumers-and-families/fircrest-residential-habilitation-center), accessed April 2022.

[^1]:    11 Email communication, K. Dedinsky, March 23, 2022.

[^2]:    13 City of Shoreline, Adopted May 16, 2023.
    City of Shoreline, 2023
    City of Shoreline website, https://www.shorelinewa.gov/government/projects-initiatives/capital-improvement-project-map, accessed November 2023.
    Email communication, K. Dedinsky, March 23, 2022.

[^3]:    17 City of Shoreline, Comprehensive Plan, Adopted December 10, 2012.
    HCM $6^{\text {th }}$ Edition, Transportation Research Board, 2016.
    19 US Department of Transportation, Federal Highway Administration, 2009.

[^4]:    20 ITE, $11^{\text {th }}$ Edition, September 2021.

[^5]:    21 Heffron Transportation, Inc., Olympia Behavioral Health Hospital, Universal Health Services, Inc., 2020. Heffron Transportation, Inc., November 14, 2006.

[^6]:    23 ITE, $3^{\text {rd }}$ Edition, Sept. 2017.

[^7]:    24 Version 6, United States Census Bureau, web-based mapping and reporting application, https://onthemap.ces.census.gov/, accessed April 2022.

[^8]:    26 Existing parking supply, proposed supply and estimated demand from AHBL, November 2023.

[^9]:    ${ }^{27}$ PLN22-0190 - MDP Review $1523015^{\text {th }}$ Ave NE - Fircrest School Master Development, Cory Johnson, April 12, 2023.

